

**CONCEPTUAL DRAINAGE PLAN**  
**For**  
**RASPBERRY ACRES**  
**2155 W STRONG ROAD**  
**SPOKANE, WA**

Prepared for:

**RASPBERRY ACRES, LLC**  
18114 N Austin Road  
Spokane, WA 99208

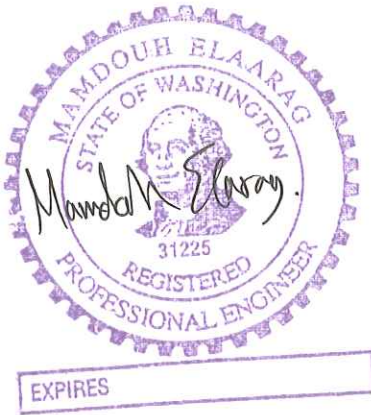
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April 17, 2021

Conceptual Drainage Plan  
Raspberry Acres  
Spokane, WA.

The data, calculations, text and graphic information contained in this document were compiled and published under the supervision and direction of the undersigned, whose seal as a professional engineer licensed to practice as such in the State of Washington, is affixed below.



5-6-21

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(Seal)

Mamdouh Elarag.  
(Consultant/Professional Engineer)

Date 5-6-21

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## I. Introduction

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### I.1. Site Description

The project site is at 2155 W Strong Road, Spokane Washington. Figure 1 – Location Map shows the proximity of the site with respect to City of Spokane and surrounding area. The subject property is parcel number 26244.0085 with approximately 6.4 acres.

### I.2. Proposed Project

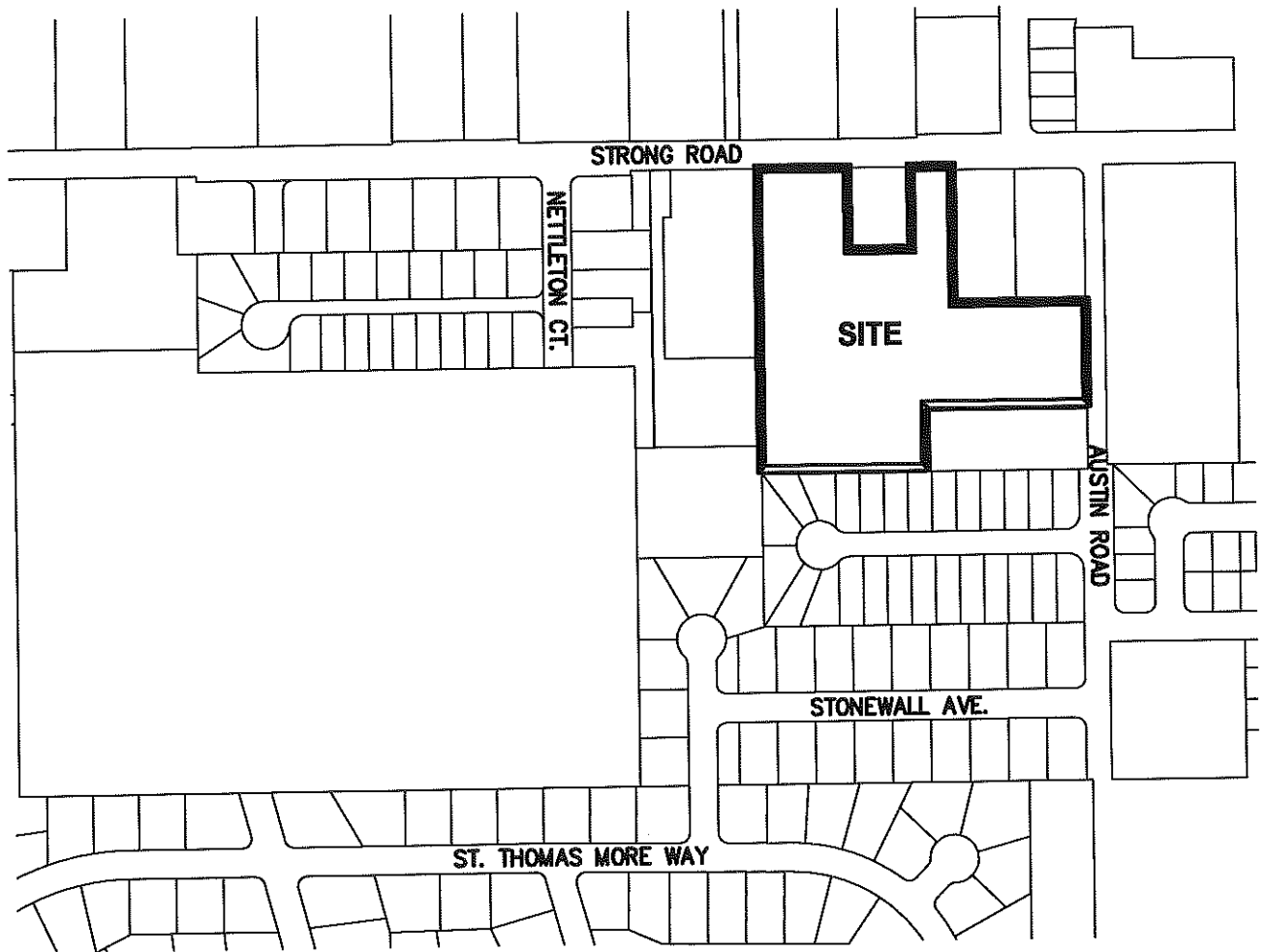
The proposed project is to develop existing parcel into thirty-one (31) single family residential lots. Construction will include clearing and grading of the site, installation of underground utilities, on-site paving and concrete work. Figure 4 – Post-Development Conditions shows the layout of the development and proposed improvements.

The project is located within the Five Mile Special District which requires a special connection agreement with the City of Spokane for use of the Austin Ravine Drainage System. The drainage system is designed to provide treatment using the '208' runoff method as described in the SRSM and disposing to the existing storm water system on Austin Road at the assigned rate by the City of Spokane.





NOT TO SCALE



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**RASPBERRY ACRES  
CITY OF SPOKANE, WASHINGTON  
DRAINAGE REPORT**

**FIGURE 1**

**SCALE: NTS**

**DRAWN BY: MHE**

**VICINITY MAP**

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## II. Background Information

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### II.1. Topography

The topography of the site slopes from a maximum elevation of approximately 2390-Ft. (NAVD 88) to a low elevation of approximately 2375-Ft. The elevations presented in Figure 3 – Pre-Development Conditions are based on a topographic survey conducted by Landtek, LLC for this project.

### II.2. Soils

The National Resources Conservation Service (NRCS), has mapped the soil in the vicinity of the project site. According to the soil survey, the project site is underlain by Brincken, moist-Uhlig complex and Seabold, warm-Brincken. These soils are described as ashy silt loam to extremely gravelly sandy loam. See Appendix A for additional soil information.

ALLWEST prepared a geotechnical report for this project dated February 10, 2020. The report indicates that soils for this project are mainly Sandy Clay and Clayey Silty Sand. The report recommends using Equation 6-1D of the SRSM to size stormwater swales for this project.

A copy of the geotechnical report is submitted.

### II.3. Drainage System Determination

The drainage system will consist of collecting the storm water, providing treatment using the '208' runoff method as described in the SRSM and disposing to the existing storm water system on Austin Road at the assigned rate by the City of Spokane. The City of Spokane assigned 20 gpm/acre for the outflow into the Austin Ravine.

### III. Drainage Narrative

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#### III.1. Introduction

This report describes the general drainage conditions on the site in relation to the storm water control requirements of City of Spokane. This design is the result of our analysis of site conditions. Design parameters are based on the requirements set forth in the City of Spokane, the Spokane Regional Storm water Manual (SRSM) and generally accepted engineering practices and theory.

Pre-development flow of any off-site runoff passing through the plat shall not be increased (rate or volume) or concentrated due to development of the plat, based on a 50-year design storm.

#### III.2. Pre-Development Analysis

In the pre-developed condition, the site is considered as three basins. The basins were determined by the natural topography of the plat. See Figure 3 – Pre-Developed Conditions in Appendix B which shows the pre-developed basins.

Pre-development storm water runoff rates for 2, 10, 50 and 100 year events were modeled using a computer software called HydroCad. The CN factor used was 80 for Soil Group C and cultivated agricultural lands for small grains.

Calculations for the 2, 10, 50 and 100 year storm events were performed (see Appendix B). The following table summarizes the pre-development runoff rates for the basin.

**Table No. 1 – Pre-Development Basin Runoff Summary**

Basin	2-Year	10-Year	50-Year	100-Year
A	1.21 CFS	1.67 CFS	2.70 CFS	3.25 CFS
B	1.06 CFS	1.47 CFS	2.38 CFS	2.87 CFS
C	0.78 CFS	1.07 CFS	1.69 CFS	2.04 CFS
<b>TOTAL</b>	<b>3.05 CFS</b>	<b>4.21 CFS</b>	<b>6.77 CFS</b>	<b>8.16 CFS</b>

#### III.3. Post-Development

All runoff within the proposed drainage basins will be collected and treated using the '208' runoff method as described in the SRSM. In the developed condition, the project includes seven (7) on-site basin (see Figure 4). Weighted "C" Runoff Coefficients were calculated for each basin of less than 10 acres as required by the SRMS. Table 1 provides the basin size, total impervious areas, and runoff coefficients for the post developed condition.

**Table No. 1 – Runoff Coefficient Summary**

Basin	Total Area (SF)	Total Area (AC)	'208' Impervious Area (SF)	Total Impervious Area (SF)	Runoff Coefficient "C"
A	6400	0.147	3690	4190	0.64
B	87480	2.00	16570	42155	0.51
C	14030	0.322	5735	6745	0.54
D	43225	0.99	12570	21370	0.52
E	42000	0.964	10880	20920	0.52
F	74470	1.71	13380	32970	0.48
G	13400	0.31	5051	7751	5649

In calculating the '208' impervious area (PGIS) the assumed driveway area was 500 square feet. An assumed roof area of 2,000 square feet per lot was used in the total impervious area.

#### III.4. '208' Calculations

The '208' storage volume for each basin was designed to adequately contain the runoff created by the first half-inch of rainfall upon the '208' impervious areas within the basin it serves. The provided '208' treatment volume shown in Table 2 is based on pond bottom areas and 3:1 side slopes at a maximum six-inch treatment depth of the swale. See Appendix "C" for swale volume calculations. Table 2 summarizes the requirements and designs of the ponds by basin.

**Table No. 2 – '208' Volume Summary**

Pond	Pond Bottom Area (SF)	'208' Volume Required (CF)	Provided Pond '208' Volume (CF)	Total Storage Volume (CF)
A	240	154	185	507
B	1035	690	781	2097
C	720	239	545	1467
D	750	524	567	1527
E	1200	453	905	2427
F	954	558	720	1935
G	360	210	275	747

A sub-basin analyses will be completed to demonstrate that the lower swale cells are adequately sized for the tributary PGIS areas.

### III.5 Larger Storm Events

An analysis was done to evaluate the effects of larger storm events or failure of proposed facilities. A visual inspection was conducted and the following was concluded:

- The proposed project engineering plans will neither aggravate an existing drainage problem nor create a new drainage problem.
- All storm water runoff from the proposed project will discharge at the natural, pre-developed location and will not adversely affect any private property.
- **The storm water system will be designed with additional storage volume capacity to handle the 100-year storm event.**

### III.6 Inlet Capacities

Inlet capacity calculations will be performed for all curb inlets to determine the stormwater runoff to be collected by each drainage structure, and the remaining by-pass flows to be addressed by the next downstream structure. By-pass flows were calculated for each inlet on a continuous grade and added to the following inlet.

Appendix "C" will include inlet capacity calculations. The inlet calculations will include a 50% clogging factor per City Design Standard 6.3-7(d).

### III.7 Roadway Flooded Width Calculations

Spokane County Stormwater Guidelines required that a minimum of 12' of non-flooded roadway surface be provided during a storm event for local access streets. Appendix "C" will include the calculated flooded roadway width.

### III.8 Post Development Analysis

The proposed Five Mile Grove development will employ a detention system which is the various swale areas which will all drain to the end of the cul-de-sac. A stormwater pump station is designed to discharge the approved outflow into the existing stormwater pipe in Austin Road. The designated outflow rate is 20gpm per acre which is equal to 128 GPM. The facility will be designed such that the release rate does not exceed the pre-developed conditions for multiple storm events. The total post-developed discharge rate shall be limited to the pre-development rates outlined in the following table:

**Allowable Discharge Rates**

Design Frequency (24 Hr Storm)	Post-developed Discharge Rate
2-year	≤ 2-year pre-developed
10-year	≤ 10-year pre-developed
50-year	≤ 50-year pre-developed
100-year	Additional Storage

Computer software called HydroCad was used. HydroCad is a computer aided design program for modeling the hydrology and hydraulics of storm water runoff. It is based largely on hydrology techniques developed by the Soil Conservation Service (now the Natural Resources Conservation Service), combined with other hydrology and hydraulics calculations. For a given rainfall event these techniques are used to generate hydrographs throughout a watershed.

HydroCad was used to generate the peak flows for each sub-basin and to determine the size of swales and pond needed to limit the discharge rates to the pre-developed rates. Each sub-basin will have a drainage swale/pond to store and route the peak flows generated and meet the allowable discharge rates listed above.

Refer to Appendix C of this report for the calculations performed as part of the design of the swales and detention pond. The following tables summarize the calculations.

**2-yr Discharge Rates**

Sub-Basins	Post-Developed Peak In (cfs)	Post-Developed Peak Out (cfs)
B	1.25	0.98
C	0.26	0.19
D	0.74	0.58
E	0.55	0.40
F	0.97	0.79
<b>TOTAL</b>	<b>3.77</b>	<b>2.94</b>

**Total post-developed peak discharge for a 2-yr storm event = 2.94 cfs minus 0.285 cfs (pump) equals 2.66 which is less than the 3.05 cfs pre-developed peak for Basins A-C.**

**10-yr Discharge Rates**

Sub-Basins	Post-Developed Peak In (cfs)	Post-Developed Peak Out (cfs)
B	1.65	1.31
C	0.34	0.25
D	0.96	0.77
E	0.73	0.55
F	1.28	1.05
<b>TOTAL</b>	<b>4.53</b>	<b>3.93</b>

**Total post-developed peak discharge for a 10-yr storm event = 3.93 cfs minus 0.285 cfs (pump) equals 3.65 which is less than the 4.21 cfs pre-developed peak for Basins A-C.**

**50-yr Discharge Rates**

Sub-Basins	Post-Developed Peak In (cfs)	Post-Developed Peak Out (cfs)
B	2.49	2.01
C	0.51	0.40
D	1.44	1.19
E	1.11	0.86
F	1.95	1.64
<b>TOTAL</b>	<b>7.5</b>	<b>6.1</b>

Total post-developed peak discharge for a 50-yr storm event = 6.1 cfs minus 0.285 cfs (pump) equals 5.82 which is less than the 6.77 cfs pre-developed peak for Basins A-C.

**100-yr Discharge Rates**

Sub-Basins	Post-Developed Peak In (cfs)	Post-Developed Peak Out (cfs)
B	2.95	2.38
C	0.60	0.47
D	1.68	1.41
E	1.31	1.03
F	2.3	1.94
<b>TOTAL</b>	<b>8.84</b>	<b>7.23</b>

Total post-developed peak discharge for a 100-yr storm event = 7.23 cfs minus 0.285 cfs (pump) equals 6.95 which is less than the 8.16 cfs pre-developed peak for Basins A-C.

**Runoff Volume Pre-Development vs. Post-Development (CF)**

Storm Event	Pre-Developed Runoff Volume Basins A-C	Post-Developed Runoff Volume Basins B-F	Post-Pre	Provided Swale Storage
2-Year	5527	8403	2876	9450
50-year	11559	16344	4785	9450
100-year	13843	19279	5436	9450

#### **IV. Conclusion**

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As demonstrated by this report and the enclosed calculations, the designed storm drainage facilities for Raspberry Acres will consist of collecting the storm water, providing treatment using the '208' runoff method as described in the SRSM and disposing to the existing storm water system on Austin Road at a lower rate than the pre-developed rate and volume.



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APPENDIX A – NRCS SOILS DATA



A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Spokane County, Washington

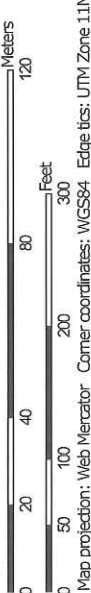
## Raspberry Acres



# Custom Soil Resource Report Soil Map



Map Scale: 1:1,670 if printed on A landscape (11" x 8.5") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 11N WGS84



## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.


Soil Survey Area: Spokane County, Washington  
 Survey Area Data: Version 12, Jun 4, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 18, 2019—Jul 23, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## MAP LEGEND

 Area of Interest (AOI)	 Spoil Area
 Soils	 Stony Spot
 Area of Interest (AOI)	 Very Stony Spot
 Soil Map Unit Polygons	 Wet Spot
 Soil Map Unit Lines	 Other
 Soil Map Unit Points	 Special Line Features
 Special Point Features	 Water Features
 Blowout	 Streams and Canals
 Borrow Pit	 Transportation
 Clay Spot	 Rails
 Closed Depression	 Interstate Highways
 Gravel Pit	 US Routes
 Gravelly Spot	 Major Roads
 Landfill	 Local Roads
 Lava Flow	 Background
 Marsh or swamp	 Aerial Photography
 Mine or Quarry	
 Miscellaneous Water	
 Perennial Water	
 Rock Outcrop	
 Saline Spot	
 Sandy Spot	
 Severely Eroded Spot	
 Sinkhole	
 Slide or Slip	
 Sodic Spot	

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
3501	Brincken, moist-Uhlig complex, 0 to 8 percent slopes	5.4	82.8%
3505	Seiboldt, warm-Brincken, moist complex, 0 to 8 percent slopes	1.0	15.7%
7140	Urban land-Uhlig, disturbed complex, 0 to 8 percent slopes	0.1	1.5%
7177	Urban land-Seiboldt, warm, disturbed-Brincken, moist, disturbed complex, 0 to 3 percent slopes	0.0	0.0%
<b>Totals for Area of Interest</b>		<b>6.5</b>	<b>100.0%</b>

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

## Spokane County, Washington

### 3501—Brincken, moist-Uhlig complex, 0 to 8 percent slopes

#### Map Unit Setting

*National map unit symbol:* qv8w  
*Elevation:* 1,900 to 2,500 feet  
*Mean annual precipitation:* 18 to 22 inches  
*Mean annual air temperature:* 46 to 52 degrees F  
*Frost-free period:* 100 to 130 days  
*Farmland classification:* All areas are prime farmland

#### Map Unit Composition

*Brincken, moist, and similar soils:* 45 percent  
*Uhlig and similar soils:* 30 percent  
*Minor components:* 25 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Brincken, Moist

##### Setting

*Landform:* Outwash terraces on loess hills  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Loess mixed with minor amounts of volcanic ash over sandy and gravelly glaciofluvial deposits over an older age of loess

##### Typical profile

*Ap - 0 to 7 inches:* ashy silt loam  
*A - 7 to 13 inches:* ashy silt loam  
*AB - 13 to 19 inches:* ashy silt loam  
*Bw - 19 to 29 inches:* ashy silt loam  
*Bt1 - 29 to 41 inches:* extremely gravelly loam  
*Bt2 - 41 to 57 inches:* very gravelly sandy clay loam  
*2Btb - 57 to 60 inches:* silty clay loam

##### Properties and qualities

*Slope:* 0 to 8 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Well drained  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to high (0.06 to 1.98 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water capacity:* Moderate (about 8.8 inches)

##### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 2e  
*Hydrologic Soil Group:* B  
*Ecological site:* F043AY511WA - Warm, Xeric, Loamy Hillsides, Mixed ash surface (Ponderosa Pine/Dry Grass) *Pinus ponderosa* / *Pseudoroegneria spicata*, *Pinus ponderosa* / *Festuca idahoensis*

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*Other vegetative classification:* ponderosa pine/Idaho fescue (CN140)

*Hydric soil rating:* No

### Description of Uhlig

#### Setting

*Landform:* Outwash terraces

*Landform position (three-dimensional):* Tread

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Parent material:* Loess mixed with minor amounts of volcanic ash over glaciofluvial deposits

#### Typical profile

*Ap1 - 0 to 4 inches:* ashy silt loam

*Ap2 - 4 to 10 inches:* ashy silt loam

*A - 10 to 18 inches:* ashy loam

*Bt1 - 18 to 32 inches:* loam

*Bt2 - 32 to 42 inches:* loam

*C - 42 to 60 inches:* very fine sandy loam

#### Properties and qualities

*Slope:* 0 to 8 percent

*Depth to restrictive feature:* More than 80 inches

*Drainage class:* Well drained

*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.57 to 1.98 in/hr)

*Depth to water table:* More than 80 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Available water capacity:* High (about 10.4 inches)

#### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 2e

*Hydrologic Soil Group:* B

*Ecological site:* F043AY511WA - Warm, Xeric, Loamy Hillsides, Mixed ash surface (Ponderosa Pine/Dry Grass) *Pinus ponderosa* / *Pseudoroegneria spicata*, *Pinus ponderosa* / *Festuca idahoensis*

*Other vegetative classification:* ponderosa pine/bluebunch wheatgrass (CN130)

*Hydric soil rating:* No

### Minor Components

#### Fourmound

*Percent of map unit:* 14 percent

*Landform:* Plateaus

*Microfeatures of landform position:* Mounds

*Down-slope shape:* Linear, convex

*Across-slope shape:* Linear, convex

*Other vegetative classification:* ponderosa pine/common snowberry (CN170)

*Hydric soil rating:* No

#### Seaboldt

*Percent of map unit:* 6 percent

*Landform:* Outwash plains on plateaus

*Landform position (three-dimensional):* Tread

## Custom Soil Resource Report

*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Other vegetative classification:* ponderosa pine/common snowberry (CN170)  
*Hydric soil rating:* No

### Nez perce

*Percent of map unit:* 5 percent  
*Landform:* Outwash terraces on loess hills  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Other vegetative classification:* ponderosa pine/bluebunch wheatgrass (CN130)  
*Hydric soil rating:* No

## 3505—Seaboldt, warm-Brincken, moist complex, 0 to 8 percent slopes

### Map Unit Setting

*National map unit symbol:* 2mdq0  
*Elevation:* 2,300 to 2,440 feet  
*Mean annual precipitation:* 18 to 20 inches  
*Mean annual air temperature:* 46 to 52 degrees F  
*Frost-free period:* 100 to 140 days  
*Farmland classification:* Prime farmland if irrigated

### Map Unit Composition

*Seaboldt, warm, and similar soils:* 60 percent  
*Brincken, moist, and similar soils:* 25 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Seaboldt, Warm

#### Setting

*Landform:* Outwash plains on plateaus  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Loess mixed with minor amounts of volcanic ash over glaciofluvial deposits over residuum from basalt

#### Typical profile

*Ap1 - 0 to 7 inches:* ashy loam  
*Ap2 - 7 to 10 inches:* ashy loam  
*Bw1 - 10 to 16 inches:* loam  
*2Bw2 - 16 to 23 inches:* sandy loam  
*2C - 23 to 28 inches:* extremely gravelly sandy loam  
*3R - 28 to 38 inches:* bedrock

#### Properties and qualities

*Slope:* 0 to 8 percent



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*Depth to restrictive feature:* 20 to 40 inches to lithic bedrock  
*Drainage class:* Well drained  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.57 to 1.98 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water capacity:* Low (about 4.0 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 3e  
*Hydrologic Soil Group:* C  
*Ecological site:* F043AY511WA - Warm, Xeric, Loamy Hillsides, Mixed ash surface (Ponderosa Pine/Dry Grass) *Pinus ponderosa* / *Pseudoroegneria spicata*,  
*Pinus ponderosa* / *Festuca idahoensis*  
*Other vegetative classification:* ponderosa pine/Idaho fescue (CN140)  
*Hydric soil rating:* No

### Description of Brincken, Moist

#### Setting

*Landform:* Outwash terraces on loess hills  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Loess mixed with minor amounts of volcanic ash over sandy and gravelly glaciofluvial deposits over an older age of loess

#### Typical profile

*Ap - 0 to 7 inches:* ashy silt loam  
*A - 7 to 13 inches:* ashy silt loam  
*AB - 13 to 19 inches:* ashy silt loam  
*Bw - 19 to 29 inches:* ashy silt loam  
*Bt1 - 29 to 41 inches:* extremely gravelly loam  
*Bt2 - 41 to 57 inches:* very gravelly sandy clay loam  
*2Btb - 57 to 60 inches:* silty clay loam

#### Properties and qualities

*Slope:* 0 to 8 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Well drained  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to high (0.06 to 1.98 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water capacity:* Moderate (about 8.8 inches)

#### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 2e  
*Hydrologic Soil Group:* B  
*Ecological site:* F043AY511WA - Warm, Xeric, Loamy Hillsides, Mixed ash surface (Ponderosa Pine/Dry Grass) *Pinus ponderosa* / *Pseudoroegneria spicata*,  
*Pinus ponderosa* / *Festuca idahoensis*  
*Other vegetative classification:* ponderosa pine/Idaho fescue (CN140)

Custom Soil Resource Report

*Hydric soil rating:* No

**Minor Components**

**Urban land**

*Percent of map unit:* 5 percent

*Hydric soil rating:* No

**Uhlig**

*Percent of map unit:* 5 percent

*Landform:* Outwash terraces

*Landform position (three-dimensional):* Tread

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Other vegetative classification:* ponderosa pine/bluebunch wheatgrass (CN130)

*Hydric soil rating:* No

**Nez perce**

*Percent of map unit:* 5 percent

*Landform:* Outwash terraces on loess hills

*Landform position (three-dimensional):* Tread

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Other vegetative classification:* ponderosa pine/bluebunch wheatgrass (CN130)

*Hydric soil rating:* No

**7140—Urban land-Uhlig, disturbed complex, 0 to 8 percent slopes**

**Map Unit Setting**

*National map unit symbol:* 2mfrn

*Elevation:* 2,350 to 2,400 feet

*Mean annual precipitation:* 18 to 20 inches

*Mean annual air temperature:* 46 to 52 degrees F

*Frost-free period:* 100 to 140 days

*Farmland classification:* Not prime farmland

**Map Unit Composition**

*Urban land:* 70 percent

*Uhlig, disturbed, and similar soils:* 20 percent

*Minor components:* 10 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

**Description of Urban Land**

**Interpretive groups**

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 8

*Hydric soil rating:* No

## Custom Soil Resource Report

### Description of Uhlig, Disturbed

#### Setting

*Landform:* Outwash terraces  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Loess mixed with minor amounts of volcanic ash over glaciofluvial deposits

#### Typical profile

*Ap1 - 0 to 4 inches:* ashy silt loam  
*Ap2 - 4 to 10 inches:* ashy silt loam  
*A - 10 to 18 inches:* ashy loam  
*Bt1 - 18 to 32 inches:* loam  
*Bt2 - 32 to 42 inches:* loam  
*C - 42 to 60 inches:* very fine sandy loam

#### Properties and qualities

*Slope:* 0 to 8 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Well drained  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high (0.20 to 0.57 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water capacity:* High (about 10.4 inches)

#### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 2e  
*Hydrologic Soil Group:* C  
*Other vegetative classification:* ponderosa pine/bluebunch wheatgrass (CN130)  
*Hydric soil rating:* No

### Minor Components

#### Seaboldt, warm, disturbed

*Percent of map unit:* 5 percent  
*Landform:* Outwash plains on plateaus  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Other vegetative classification:* ponderosa pine/Idaho fescue (CN140)  
*Hydric soil rating:* No

#### Brincken, moist, disturbed

*Percent of map unit:* 3 percent  
*Landform:* Outwash terraces on loess hills  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Other vegetative classification:* ponderosa pine/Idaho fescue (CN140)  
*Hydric soil rating:* No

## Custom Soil Resource Report

### **Nez perce, disturbed**

*Percent of map unit:* 2 percent

*Landform:* Plateaus

*Landform position (two-dimensional):* Summit

*Landform position (three-dimensional):* Interfluve

*Down-slope shape:* Linear

*Across-slope shape:* Convex

*Other vegetative classification:* ponderosa pine/bluebunch wheatgrass (CN130)

*Hydric soil rating:* No

## **7177—Urban land-Seaboldt, warm, disturbed-Brincken, moist, disturbed complex, 0 to 3 percent slopes**

### **Map Unit Setting**

*National map unit symbol:* 2mdp2

*Elevation:* 2,270 to 2,400 feet

*Mean annual precipitation:* 18 inches

*Mean annual air temperature:* 46 to 52 degrees F

*Frost-free period:* 100 to 140 days

*Farmland classification:* Not prime farmland

### **Map Unit Composition**

*Urban land:* 45 percent

*Seaboldt, warm, disturbed, and similar soils:* 25 percent

*Brincken, moist, disturbed, and similar soils:* 20 percent

*Minor components:* 10 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

### **Description of Urban Land**

#### **Interpretive groups**

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 8

*Hydric soil rating:* No

### **Description of Seaboldt, Warm, Disturbed**

#### **Setting**

*Landform:* Outwash plains on plateaus

*Landform position (three-dimensional):* Tread

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Parent material:* Loess mixed with minor amounts of volcanic ash over glaciofluvial deposits over residuum from basalt

#### **Typical profile**

*Ap1 - 0 to 7 inches:* ashy loam

*Ap2 - 7 to 10 inches:* ashy loam

## Custom Soil Resource Report

*Bw1 - 10 to 16 inches: loam*  
*2Bw2 - 16 to 23 inches: sandy loam*  
*2C - 23 to 28 inches: extremely gravelly sandy loam*  
*3R - 28 to 38 inches: bedrock*

### Properties and qualities

*Slope: 0 to 3 percent*  
*Depth to restrictive feature: 20 to 40 inches to lithic bedrock*  
*Drainage class: Well drained*  
*Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)*  
*Depth to water table: More than 80 inches*  
*Frequency of flooding: None*  
*Frequency of ponding: None*  
*Available water capacity: Low (about 4.0 inches)*

### Interpretive groups

*Land capability classification (irrigated): None specified*  
*Land capability classification (nonirrigated): 3s*  
*Hydrologic Soil Group: C*  
*Ecological site: F043AY511WA - Warm, Xeric, Loamy Hillsides, Mixed ash surface (Ponderosa Pine/Dry Grass) Pinus ponderosa / Pseudoroegneria spicata, Pinus ponderosa / Festuca idahoensis*  
*Other vegetative classification: ponderosa pine/Idaho fescue (CN140)*  
*Hydric soil rating: No*

## Description of Brincken, Moist, Disturbed

### Setting

*Landform: Outwash terraces on loess hills*  
*Landform position (three-dimensional): Tread*  
*Down-slope shape: Linear*  
*Across-slope shape: Linear*  
*Parent material: Loess mixed with minor amounts of volcanic ash over sandy and gravelly glaciofluvial deposits over an older age of loess*

### Typical profile

*Ap - 0 to 7 inches: ashy silt loam*  
*A - 7 to 13 inches: ashy silt loam*  
*AB - 13 to 19 inches: ashy silt loam*  
*Bw - 19 to 29 inches: ashy silt loam*  
*Bt1 - 29 to 41 inches: extremely gravelly loam*  
*Bt2 - 41 to 57 inches: very gravelly sandy clay loam*  
*2Btb - 57 to 60 inches: silty clay loam*

### Properties and qualities

*Slope: 0 to 3 percent*  
*Depth to restrictive feature: More than 80 inches*  
*Drainage class: Well drained*  
*Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.57 in/hr)*  
*Depth to water table: More than 80 inches*  
*Frequency of flooding: None*  
*Frequency of ponding: None*  
*Available water capacity: Moderate (about 8.8 inches)*

## Custom Soil Resource Report

### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 2e

*Hydrologic Soil Group:* C

*Other vegetative classification:* ponderosa pine/Idaho fescue (CN140)

*Hydric soil rating:* No

### Minor Components

#### Nez perce, disturbed

*Percent of map unit:* 5 percent

*Landform:* Plateaus

*Landform position (two-dimensional):* Summit

*Landform position (three-dimensional):* Interfluve

*Down-slope shape:* Linear

*Across-slope shape:* Convex

*Other vegetative classification:* ponderosa pine/bluebunch wheatgrass (CN130)

*Hydric soil rating:* No

#### Uhlig, disturbed

*Percent of map unit:* 3 percent

*Landform:* Outwash terraces

*Landform position (three-dimensional):* Tread

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Other vegetative classification:* ponderosa pine/bluebunch wheatgrass (CN130)

*Hydric soil rating:* No

#### Stutler, disturbed

*Percent of map unit:* 2 percent

*Landform:* Outwash plains

*Landform position (three-dimensional):* Tread

*Down-slope shape:* Linear

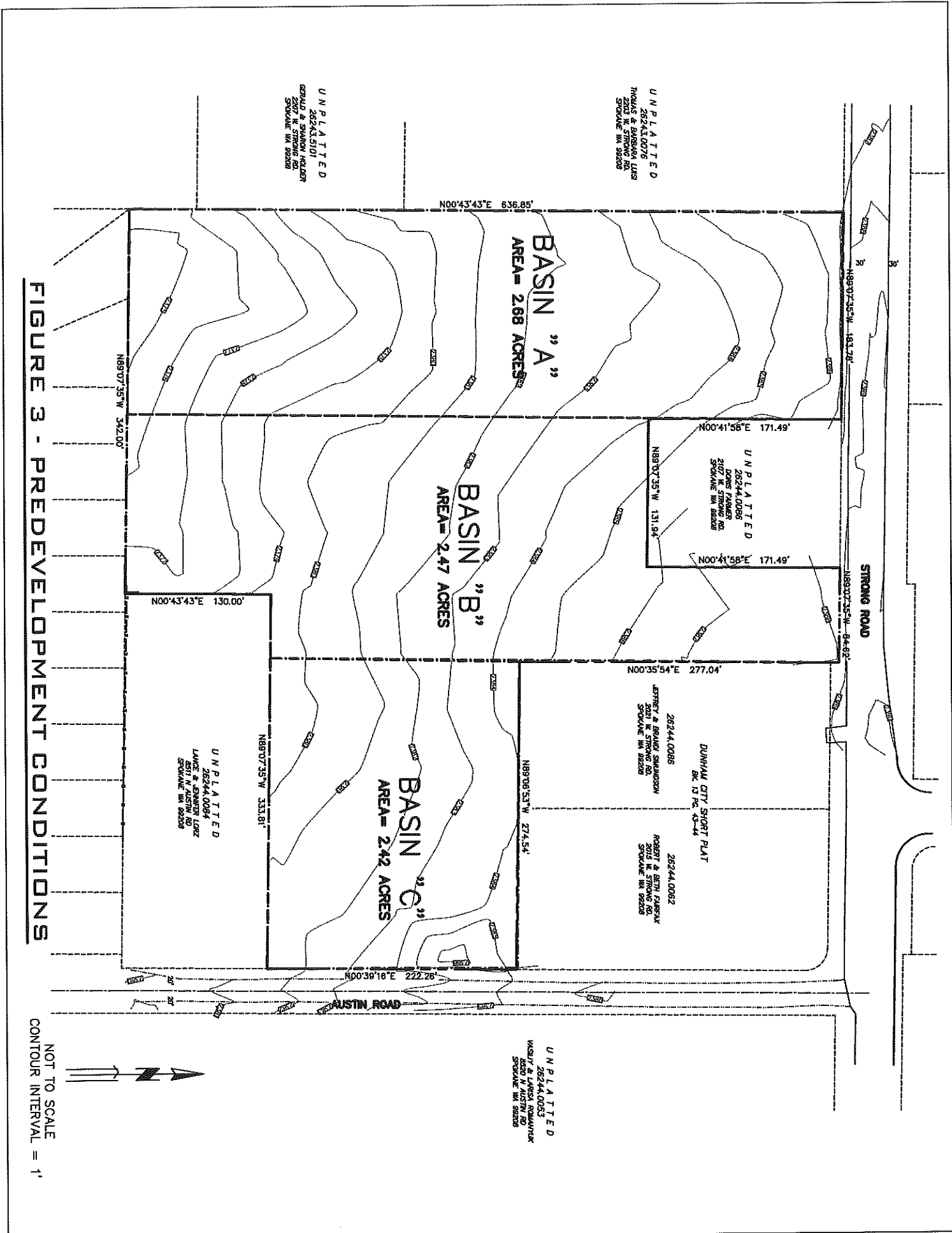
*Across-slope shape:* Linear

*Other vegetative classification:* ponderosa pine/common snowberry (CN170)

*Hydric soil rating:* No

---

APPENDIX B – PRE-DEVELOPMENT CONDITIONS & CALCULATIONS



**FIGURE 3 - PREDEVELOPMENT CONDITIONS**



### **Pre-Developed Basin A**

Approximate Total Area = 2.68 acres.

#### **Tc:**

The length to determine time of concentration = 600'  
Slope = 0.02 ft/ft  
Tc= 10.1 minutes

#### **Cn:**

From the soils map 100% of the basin is Group C with a Cn number of 80.

Weighted Cn = **80**

### **Pre-Developed Basin B**

Approximate Total Area = 2.47 acres.

#### **Tc:**

The length to determine time of concentration = 650'  
Slope = 0.0185 ft/ft  
Tc= 11.4 minutes

#### **Cn:**

From the soils map 100% of the basin is Group C with a Cn number of 80.

Weighted Cn = **80**

### Pre-Developed Basin C

Approximate Total Area = 1.41 acres.

**Tc:**

The length to determine time of concentration = 290'

Slope = 0.017 ft/ft

Tc= 5.3 minutes

**Cn:**

From the soils map 100% of the basin is Group C with a Cn number of 80.

Weighted Cn = **80**

**RASPBERRY ACRES PRE A**

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Type II 24-hr 2-YR Rainfall=1.60"

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**Summary for Subcatchment 1S: PRE BASIN A**

Runoff = 1.21 cfs @ 12.04 hrs, Volume= 2,877 cf, Depth> 0.30"

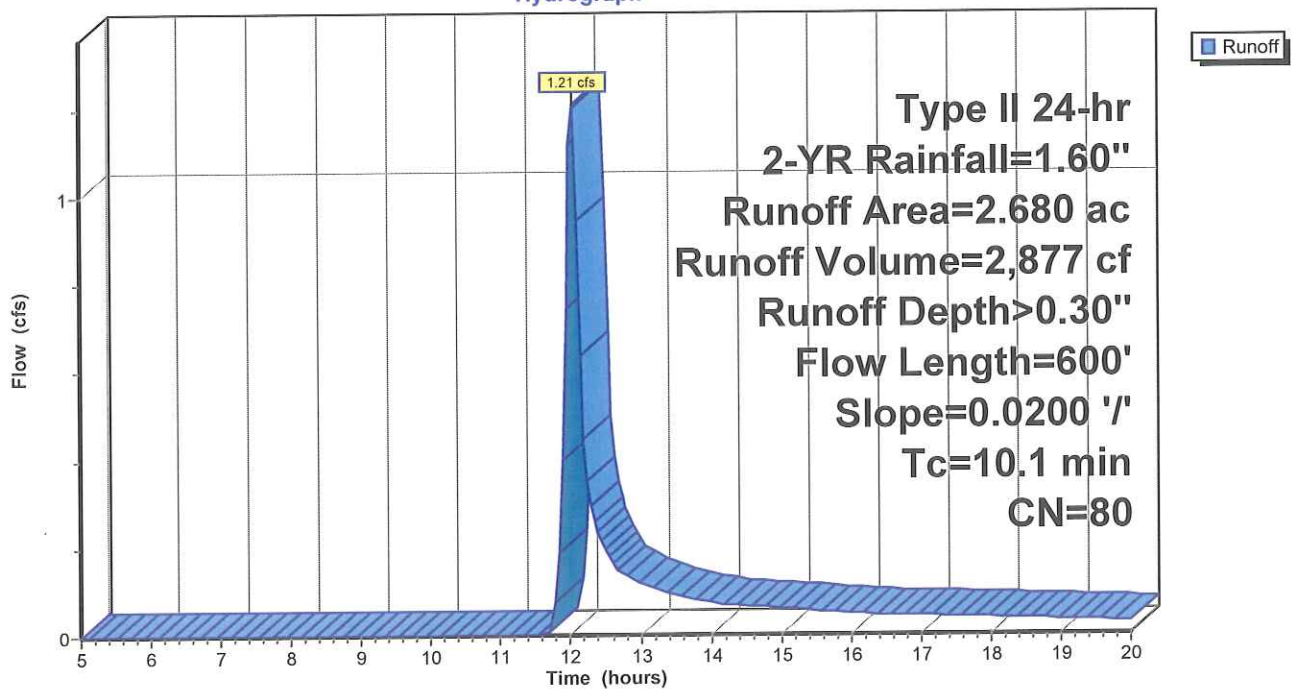
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2-YR Rainfall=1.60"

Area (ac)	CN	Description
* 2.680	80	
2.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.1	600	0.0200	0.99		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

**Subcatchment 1S: PRE BASIN A**

Hydrograph



**RASPBERRY ACRES PRE A**

Type II 24-hr 10-YR Rainfall=1.80"

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**Summary for Subcatchment 1S: PRE BASIN A**

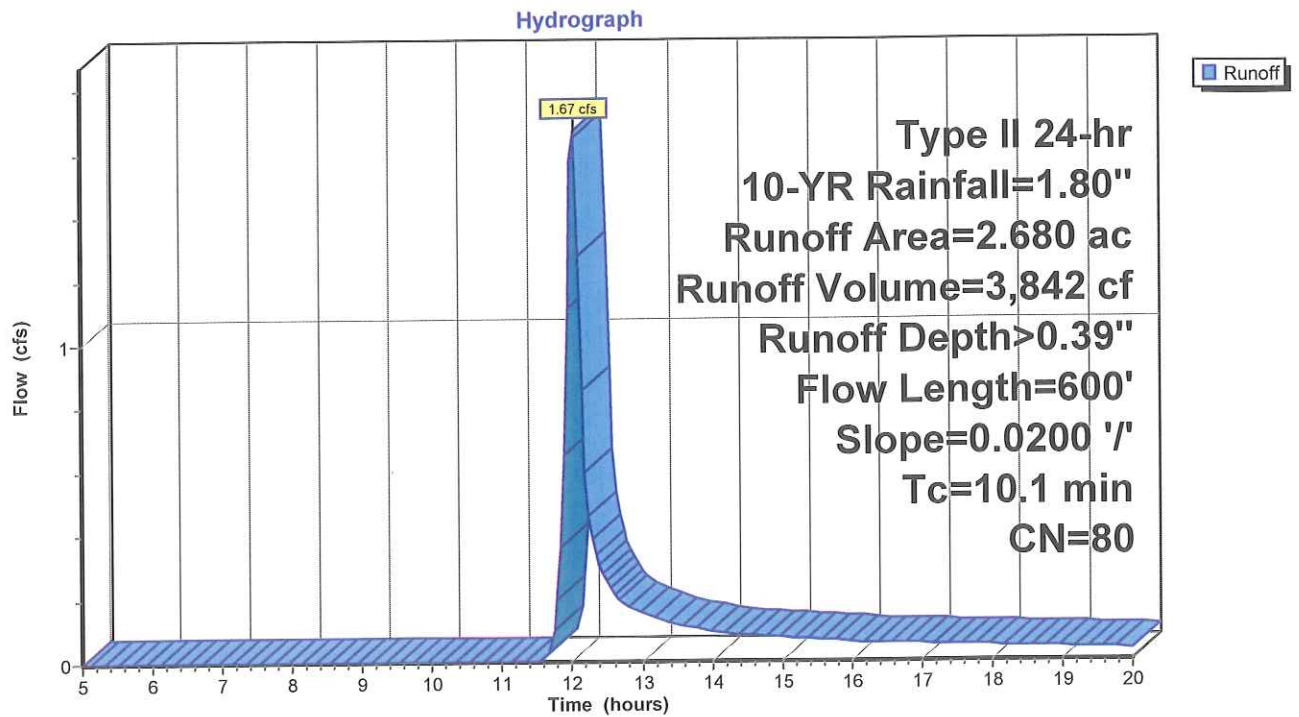
Runoff = 1.67 cfs @ 12.03 hrs, Volume= 3,842 cf, Depth> 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-YR Rainfall=1.80"

Area (ac)	CN	Description
* 2.680	80	
2.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.1	600	0.0200	0.99		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

**Subcatchment 1S: PRE BASIN A**



# RASPBERRY ACRES PRE A

Type II 24-hr 50-YR Rainfall=2.20"

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## Summary for Subcatchment 1S: PRE BASIN A

Runoff = 2.70 cfs @ 12.03 hrs, Volume= 6,017 cf, Depth> 0.62"

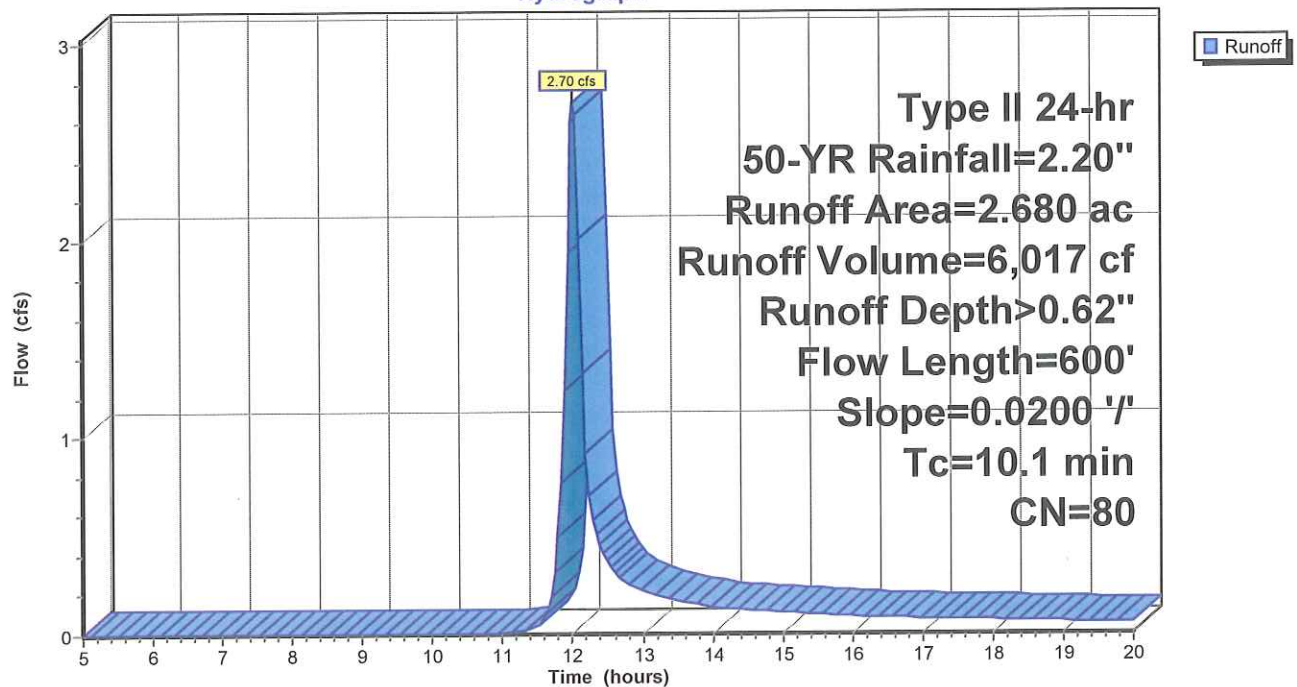
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-YR Rainfall=2.20"

Area (ac)	CN	Description
* 2.680	80	
2.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.1	600	0.0200	0.99		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

## Subcatchment 1S: PRE BASIN A

Hydrograph



**RASPBERRY ACRES PRE A**

Type II 24-hr 100-YR Rainfall=2.40"

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**Summary for Subcatchment 1S: PRE BASIN A**

Runoff = 3.25 cfs @ 12.03 hrs, Volume= 7,206 cf, Depth> 0.74"

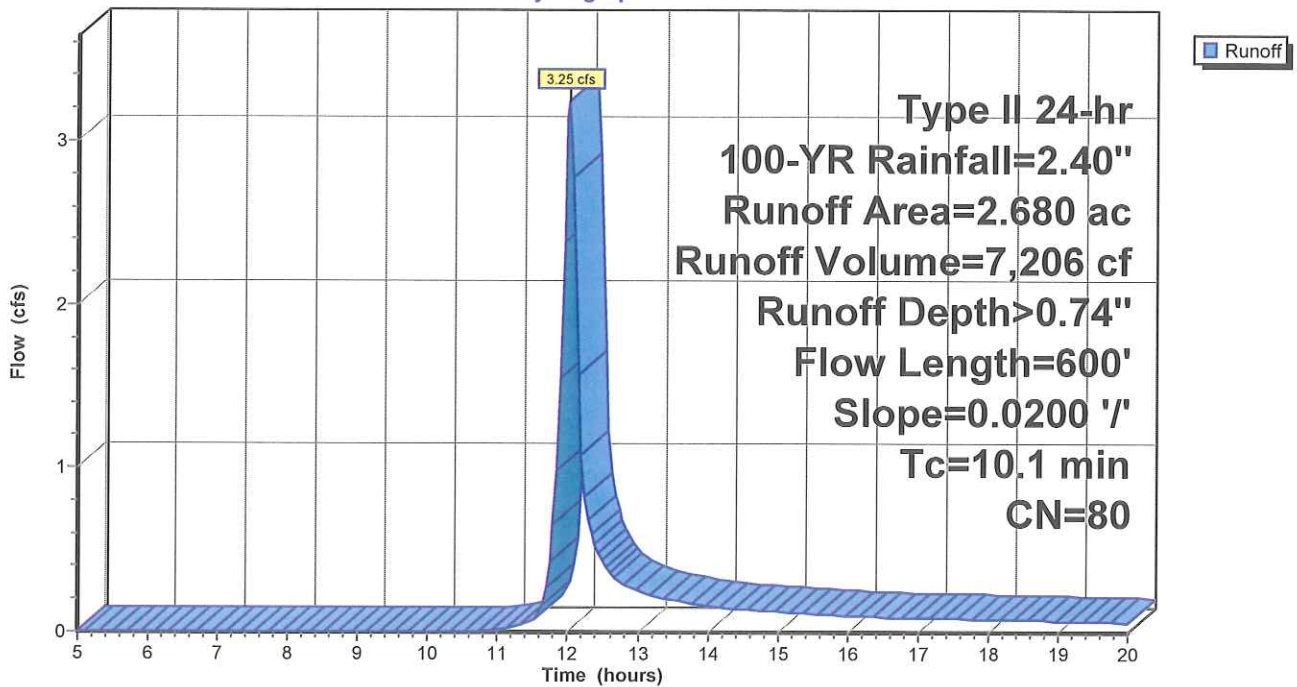
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-YR Rainfall=2.40"

Area (ac)	CN	Description
* 2.680	80	
2.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.1	600	0.0200	0.99		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

**Subcatchment 1S: PRE BASIN A**

Hydrograph





# RASPBERRY ACRES PRE B

Type II 24-hr 2-YR Rainfall=1.60"

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## Summary for Subcatchment 1S: PRE BASIN B

Runoff = 1.06 cfs @ 12.05 hrs, Volume= 2,650 cf, Depth> 0.30"

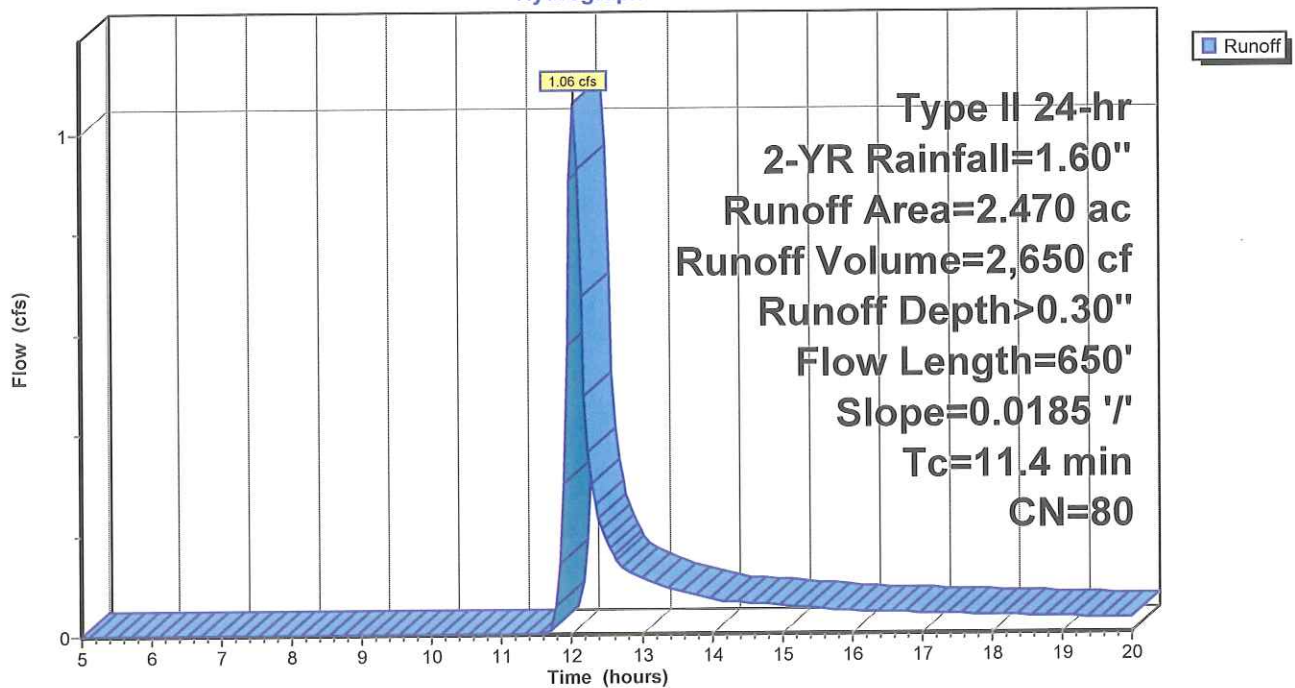
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2-YR Rainfall=1.60"

Area (ac)	CN	Description
* 2.470	80	
2.470		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.4	650	0.0185	0.95		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

## Subcatchment 1S: PRE BASIN B

Hydrograph



# RASPBERRY ACRES PRE B

Type II 24-hr 10-YR Rainfall=1.80"

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## Summary for Subcatchment 1S: PRE BASIN B

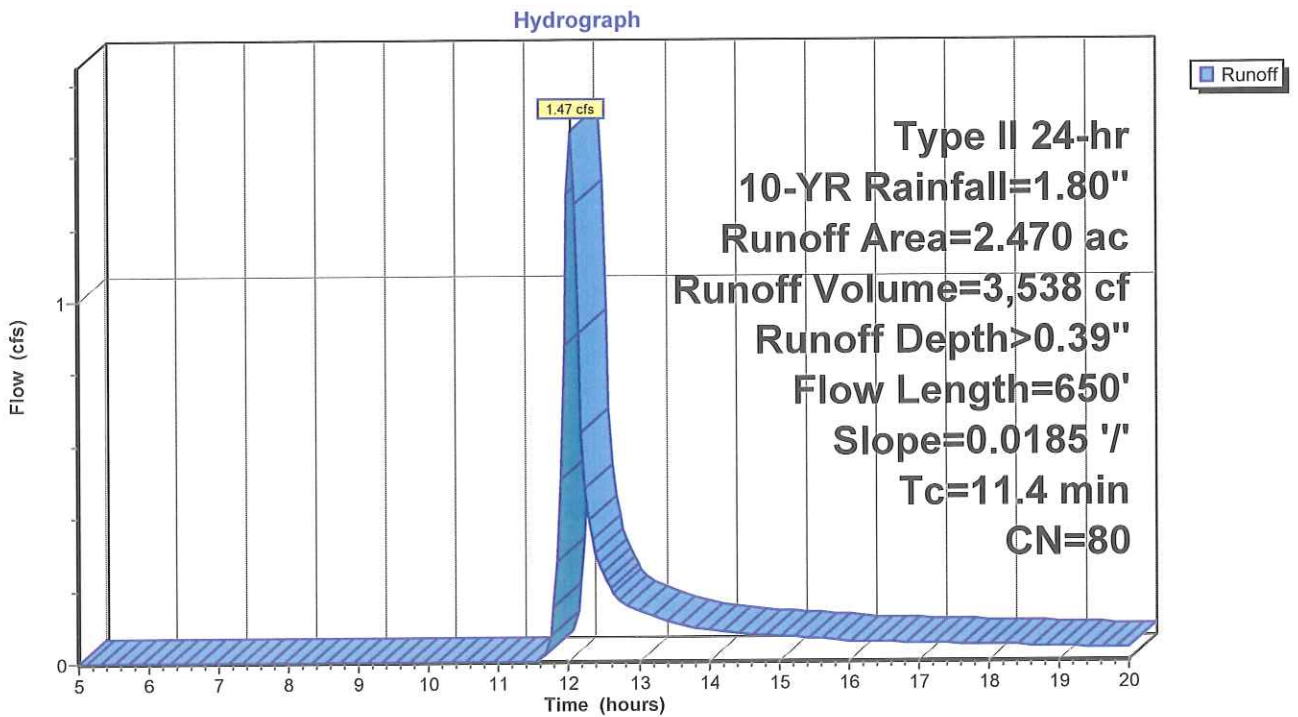
Runoff = 1.47 cfs @ 12.05 hrs, Volume= 3,538 cf, Depth> 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-YR Rainfall=1.80"

Area (ac)	CN	Description
* 2.470	80	
2.470		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.4	650	0.0185	0.95		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

## Subcatchment 1S: PRE BASIN B





**RASPBERRY ACRES PRE B**

Type II 24-hr 50-YR Rainfall=2.20"

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**Summary for Subcatchment 1S: PRE BASIN B**

Runoff = 2.38 cfs @ 12.04 hrs, Volume= 5,542 cf, Depth> 0.62"

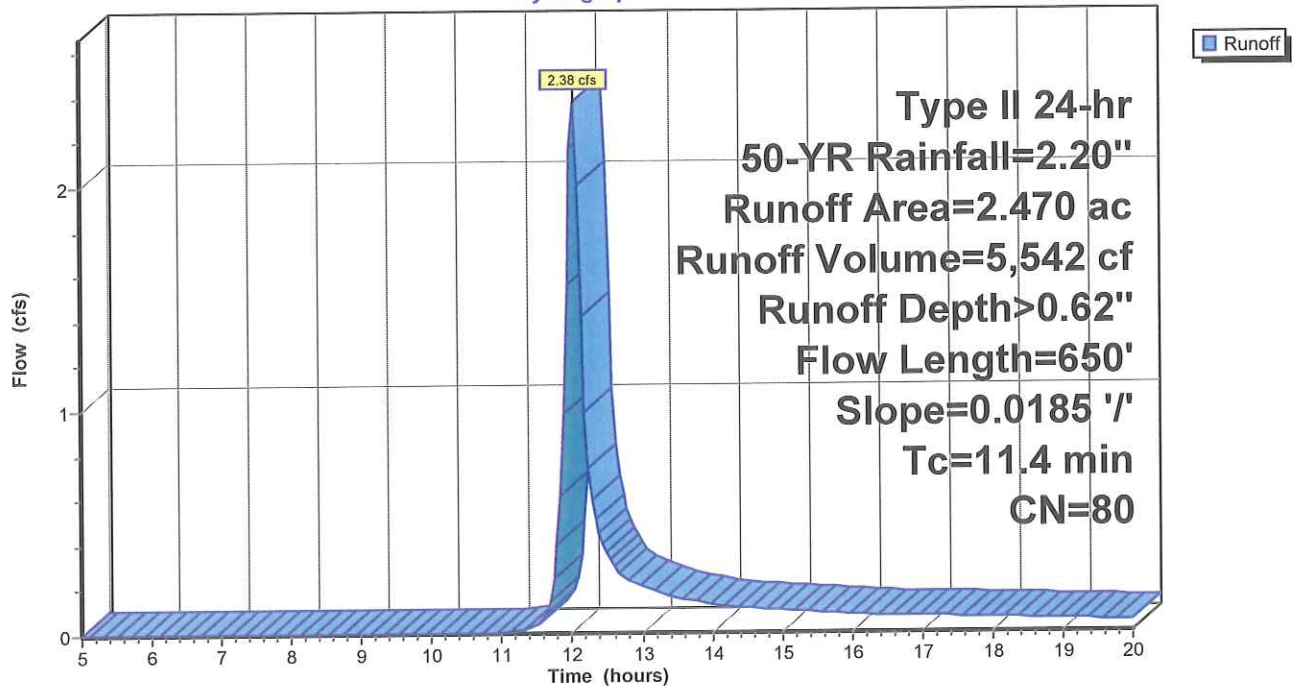
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-YR Rainfall=2.20"

Area (ac)	CN	Description
* 2.470	80	
2.470		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.4	650	0.0185	0.95		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

**Subcatchment 1S: PRE BASIN B**

Hydrograph



**RASPBERRY ACRES PRE B**

Type II 24-hr 100-YR Rainfall=2.40"

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**Summary for Subcatchment 1S: PRE BASIN B**

Runoff = 2.87 cfs @ 12.04 hrs, Volume= 6,637 cf, Depth> 0.74"

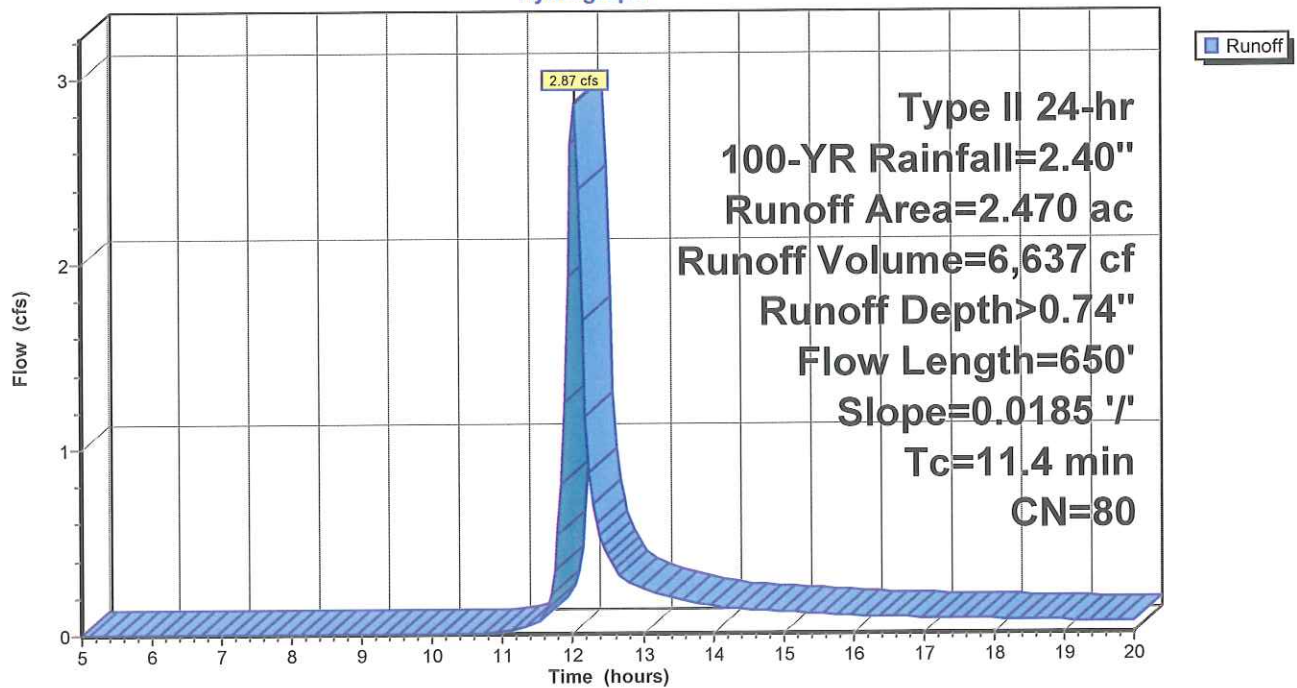
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 100-YR Rainfall=2.40"

Area (ac)	CN	Description
* 2.470	80	
2.470		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.4	650	0.0185	0.95		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

**Subcatchment 1S: PRE BASIN B**

Hydrograph



**RASPBERRY ACRES PRE C**

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Type II 24-hr 2-YR Rainfall=1.60"

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**Summary for Subcatchment 1S: PRE BASIN C**

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.78 cfs @ 11.98 hrs, Volume= 1,518 cf, Depth> 0.30"

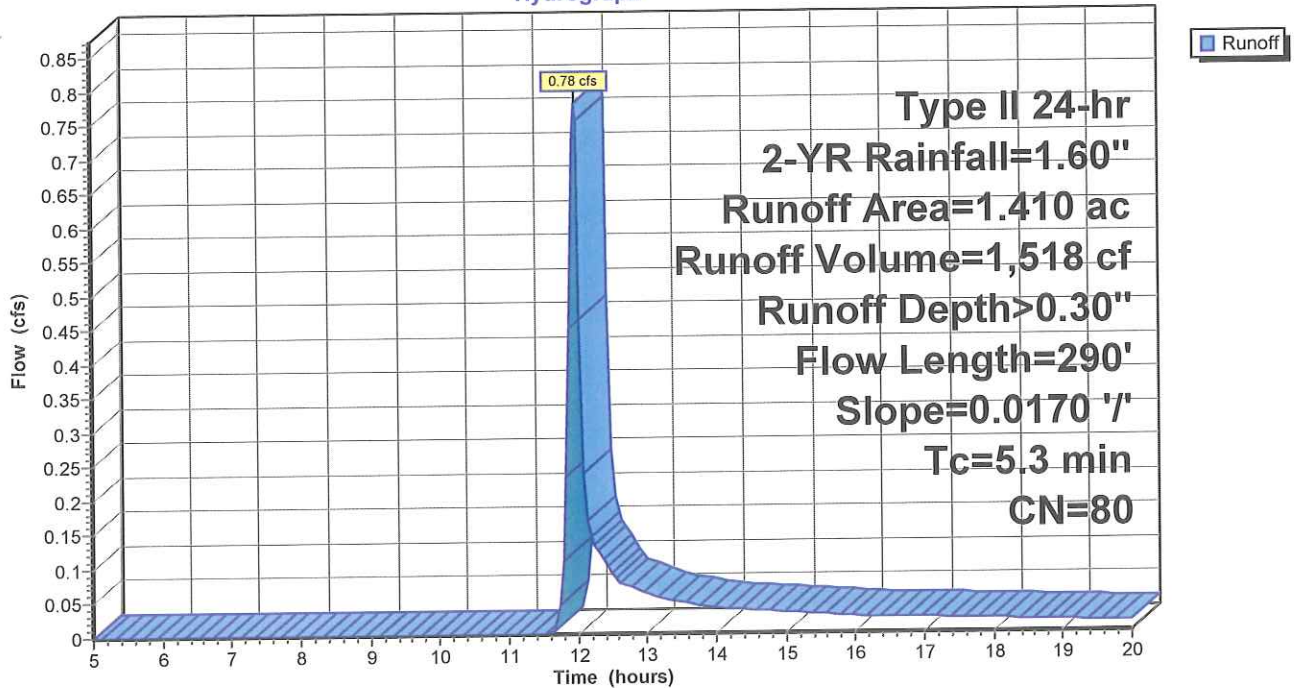
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2-YR Rainfall=1.60"

Area (ac)	CN	Description
* 1.410	80	
1.410		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.3	290	0.0170	0.91		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

**Subcatchment 1S: PRE BASIN C**

Hydrograph



**RASPBERRY ACRES PRE C**

Type II 24-hr 10-YR Rainfall=1.80"

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**Summary for Subcatchment 1S: PRE BASIN C**

[49] Hint: Tc<2dt may require smaller dt

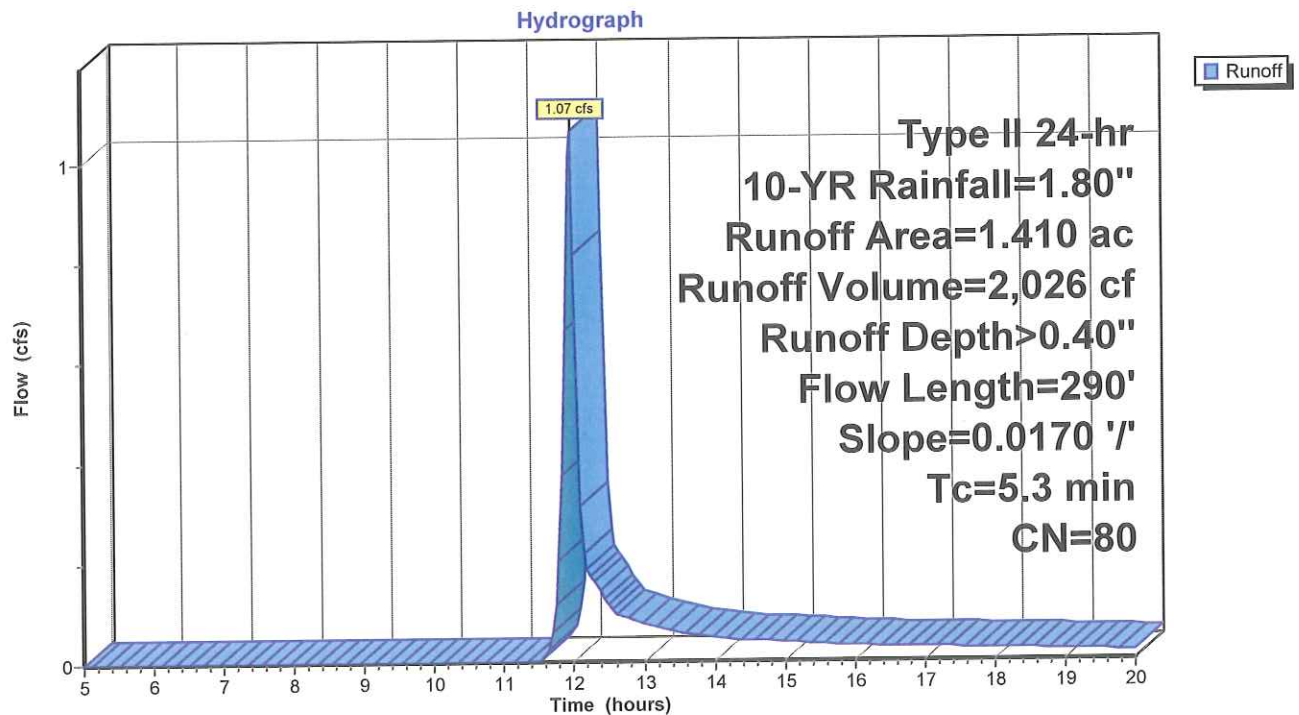
Runoff = 1.07 cfs @ 11.98 hrs, Volume= 2,026 cf, Depth> 0.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-YR Rainfall=1.80"

Area (ac)	CN	Description
* 1.410	80	
1.410		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.3	290	0.0170	0.91		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

**Subcatchment 1S: PRE BASIN C**





# RASPBERRY ACRES PRE C

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Type II 24-hr 50-YR Rainfall=2.20"

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## Summary for Subcatchment 1S: PRE BASIN C

[49] Hint:  $T_c < 2dt$  may require smaller dt

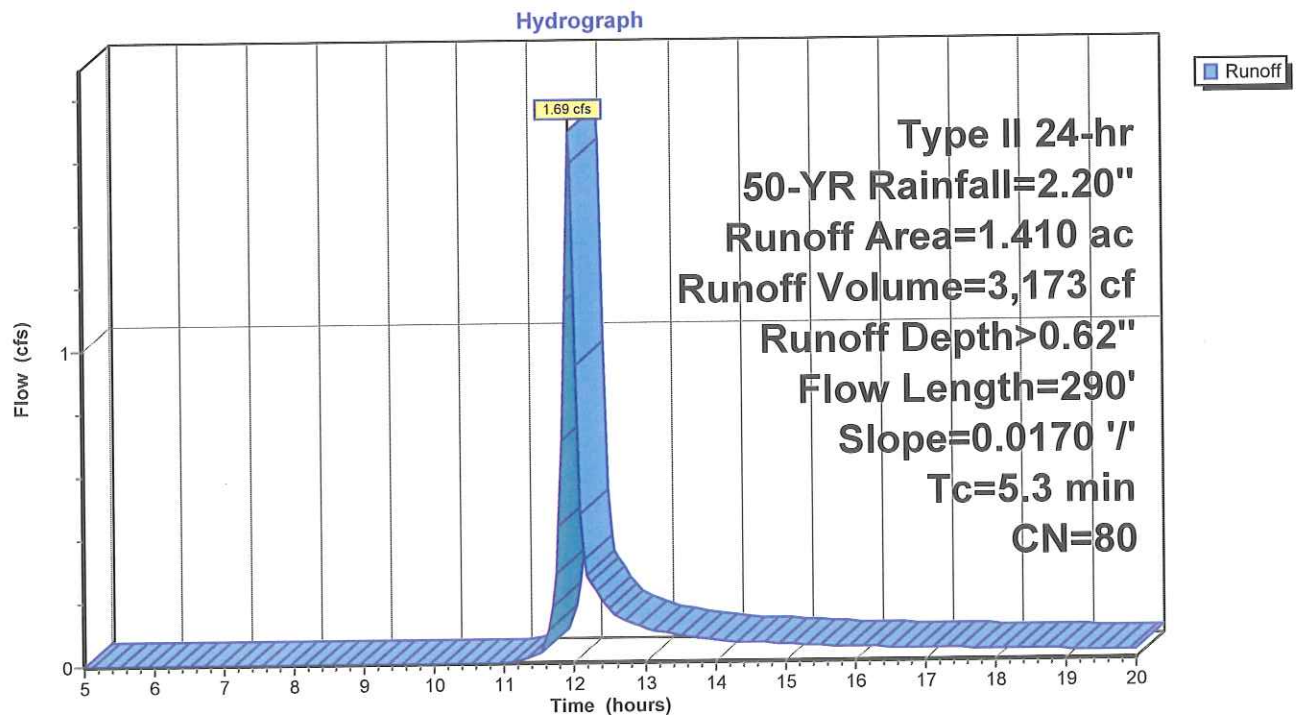
Runoff = 1.69 cfs @ 11.97 hrs, Volume= 3,173 cf, Depth > 0.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-YR Rainfall=2.20"

Area (ac)	CN	Description
* 1.410	80	
1.410		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.3	290	0.0170	0.91		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

## Subcatchment 1S: PRE BASIN C



**RASPBERRY ACRES PRE C**

Type II 24-hr 100-YR Rainfall=2.40"

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**Summary for Subcatchment 1S: PRE BASIN C**

[49] Hint: Tc<2dt may require smaller dt

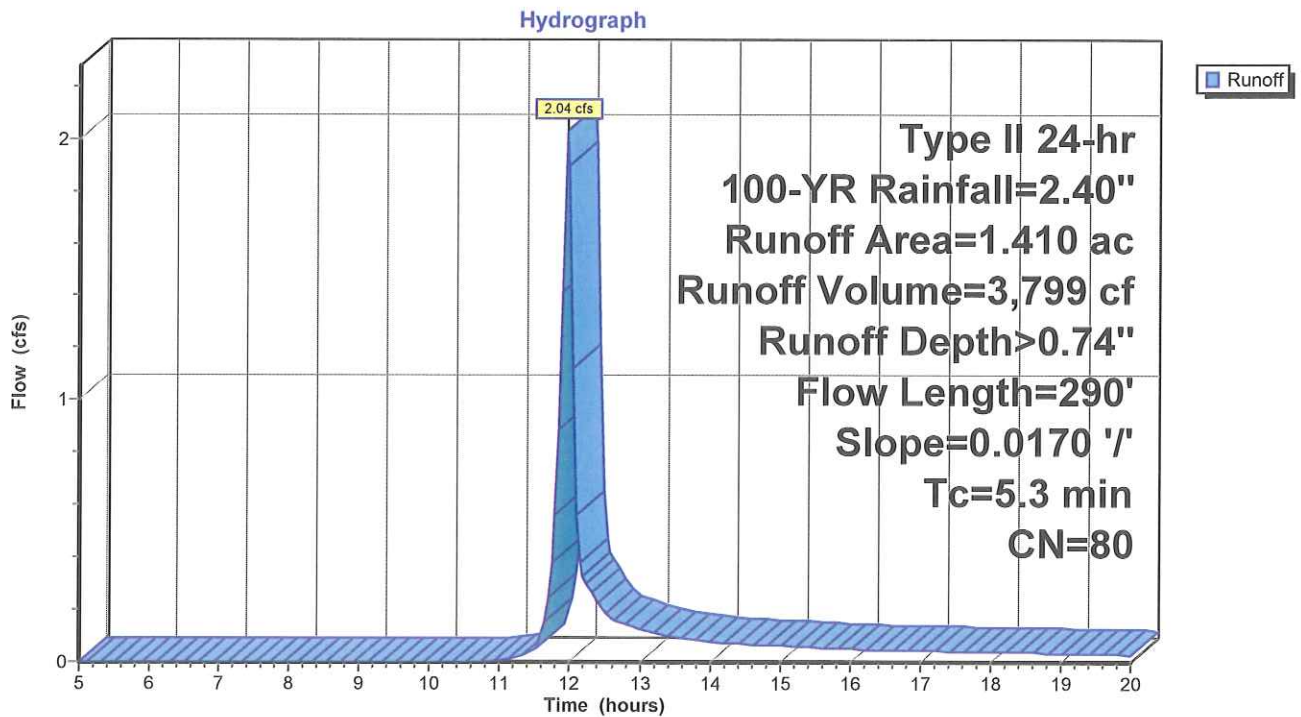
Runoff = 2.04 cfs @ 11.97 hrs, Volume= 3,799 cf, Depth> 0.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-YR Rainfall=2.40"

Area (ac)	CN	Description
* 1.410	80	
1.410		100.00% Pervious Area

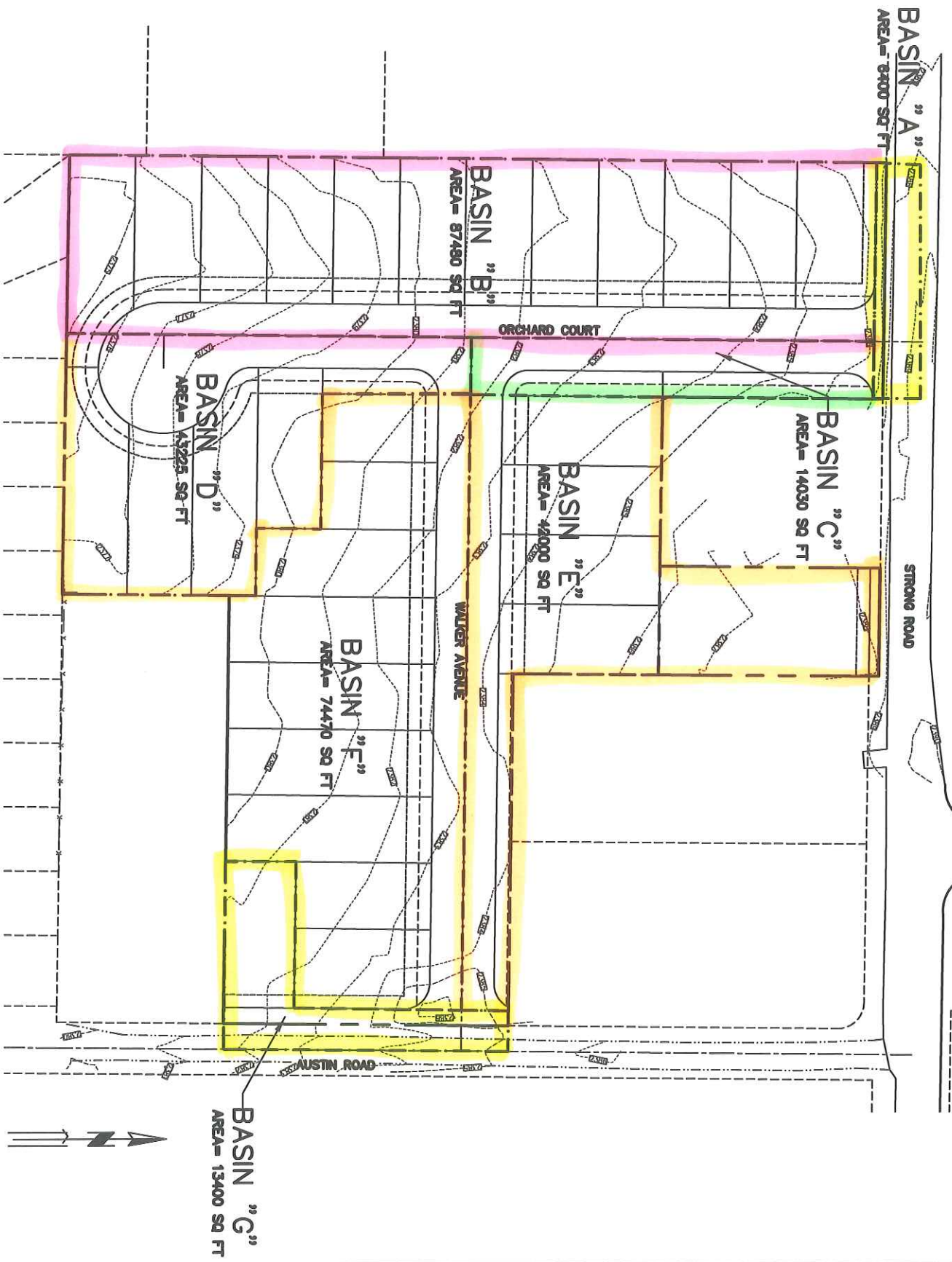
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.3	290	0.0170	0.91		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps

**Subcatchment 1S: PRE BASIN C**



---

APPENDIX C – POST-DEVELOPMENT CONDITIONS & CALCULATIONS



**FIGURE 4 - POSTDEVELOPMENT CONDITIONS**

NOT TO SCALE  
CONTOUR INTERVAL = 1'





**BASIN "A"**

Total Area = 6400 sf = 0.147 acres.

Roof Area

0

Paved Area (including curb & gutter)

180' x 20.5' = 3690 Ft<sup>2</sup>

Total Paved Area = 3690 Ft<sup>2</sup>

C=0.90

Concrete Sidewalk

100' x 5' = 500 Ft<sup>2</sup>

C=0.90

Lawns

6400 - 4190 = 2210 sf

C=0.15

Weighted "C" Factor

(0.9 x 4190) + (0.15 x 2210) divided by 6400

**= 0.64**

Required Swale Volume

V = 1815 A, where

V= Volume of swale (cubic feet)

A= Pollution generating impervious surface (acres)

V = 1815 x 0.085 acres

**= 154 CF**

Provided Swale Volume = 185 CF

Swale Along Strong Road	
Pond Side Slope	3 :1
Bottom Length (ft)	80
Bottom Width (ft)	3
Bottom Area (SF)	240
Treatment Depth (ft)	0.5
Treatment Area (SF)	498
Treatment Volume (CF)	185
Storage Depth (ft)	1
Storage Area (SF)	774
Storage Volume (CF)	507

**BASIN "B"**

Total Area = 87480 sf = 2.00 acres.

Roof Area

$$(2000 \text{ sf} \times 12) = 24,000 \text{ sf} \quad C=0.90$$

Paved Area (includes curb & gutter)

$$(533.5' \times 18.5') + 700 = 10,570 \text{ Ft}^2$$

$$\text{Total Paved Area} = 10,570 \text{ Ft}^2 \quad C=0.90$$

Concrete Driveways & Sidewalk

$$500\text{sf} \times 12 = 6,000 \text{ Ft}^2 \quad C=0.90$$

$$317' \times 5' = 1585 \text{ Ft}^2$$

Lawns

$$87480 - 42155 = 45325 \text{ sf} \quad C=0.15$$

Weighted "C" Factor

$$(0.9 \times 42155) + (0.15 \times 45325) \text{ divided by } 87480$$

$$= 0.51$$

Required Swale Volume

V = 1815 A, where

V= Volume of swale (cubic feet)

A= Pollution generating impervious surface (acres)

$$V = 1815 \times 0.38 \text{ acres}$$

$$=690 \text{ CF}$$

Provided swale volume = 781 CF

Swale Along West Side of Orchard CT.	
Pond Side Slope	3 :1
Bottom Length (ft)	345
Bottom Width (ft)	3
Bottom Area (SF)	1035
Treatment Depth (ft)	0.5
Treatment Area (SF)	2088
Treatment Volume (CF)	781
Storage Depth (ft)	1
Storage Area (SF)	3159
Storage Volume (CF)	2097

**RASPBERRY ACRES POST B**

Type II 24-hr 2-YR Rainfall=1.60"

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Page 1

**Summary for Pond 2P: SWALE B**

Inflow Area = 87,120 sf, 38.00% Impervious, Inflow Depth > 0.39" for 2-YR event  
 Inflow = 1.25 cfs @ 12.03 hrs, Volume= 2,836 cf  
 Outflow = 0.98 cfs @ 12.10 hrs, Volume= 2,809 cf, Atten= 22%, Lag= 4.2 min  
 Primary = 0.98 cfs @ 12.10 hrs, Volume= 2,809 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.29' @ 12.10 hrs Surf.Area= 1,638 sf Storage= 384 cf

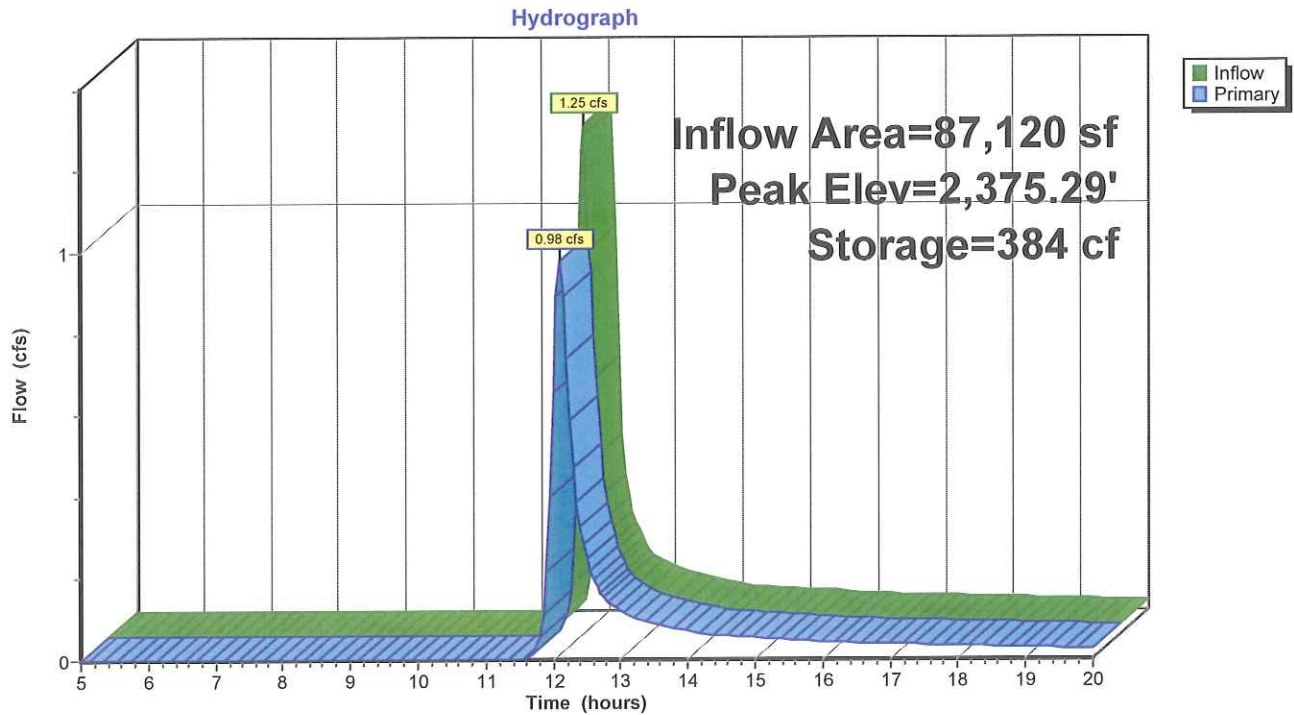
Plug-Flow detention time= 10.3 min calculated for 2,800 cf (99% of inflow)  
 Center-of-Mass det. time= 6.9 min ( 825.9 - 819.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	2,091 cf	3.00'W x 345.00'L x 1.00'H Prismaoid Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.98 cfs @ 12.10 hrs HW=2,375.29' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 0.98 cfs @ 1.75 fps)

**Pond 2P: SWALE B**



**RASPBERRY ACRES POST B**

Type II 24-hr 10-YR Rainfall=1.80"

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Page 2

**Summary for Pond 2P: SWALE B**

Inflow Area = 87,120 sf, 38.00% Impervious, Inflow Depth > 0.51" for 10-YR event  
 Inflow = 1.65 cfs @ 12.03 hrs, Volume= 3,668 cf  
 Outflow = 1.31 cfs @ 12.09 hrs, Volume= 3,638 cf, Atten= 21%, Lag= 4.0 min  
 Primary = 1.31 cfs @ 12.09 hrs, Volume= 3,638 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.35' @ 12.09 hrs Surf.Area= 1,770 sf Storage= 491 cf

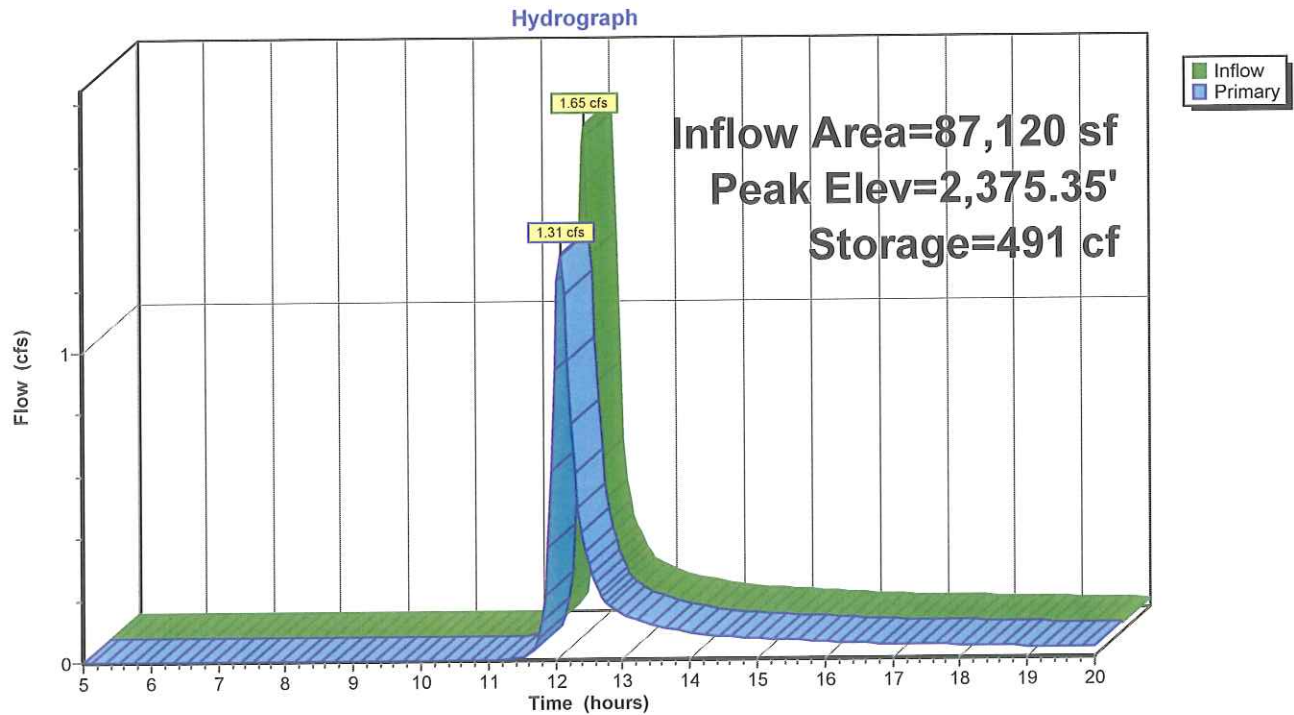
Plug-Flow detention time= 9.7 min calculated for 3,638 cf (99% of inflow)  
 Center-of-Mass det. time= 6.5 min ( 819.8 - 813.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	2,091 cf	3.00'W x 345.00'L x 1.00'H Prismaoid Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.30 cfs @ 12.09 hrs HW=2,375.35' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 1.30 cfs @ 1.93 fps)

**Pond 2P: SWALE B**





**RASPBERRY ACRES POST B**

Type II 24-hr 50-YR Rainfall=2.20"

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**Summary for Pond 2P: SWALE B**

Inflow Area = 87,120 sf, 38.00% Impervious, Inflow Depth > 0.76" for 50-YR event  
 Inflow = 2.49 cfs @ 12.02 hrs, Volume= 5,501 cf  
 Outflow = 2.01 cfs @ 12.09 hrs, Volume= 5,464 cf, Atten= 19%, Lag= 3.9 min  
 Primary = 2.01 cfs @ 12.09 hrs, Volume= 5,464 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.47' @ 12.09 hrs Surf.Area= 2,025 sf Storage= 719 cf

Plug-Flow detention time= 8.8 min calculated for 5,446 cf (99% of inflow)  
 Center-of-Mass det. time= 6.2 min ( 810.9 - 804.7 )

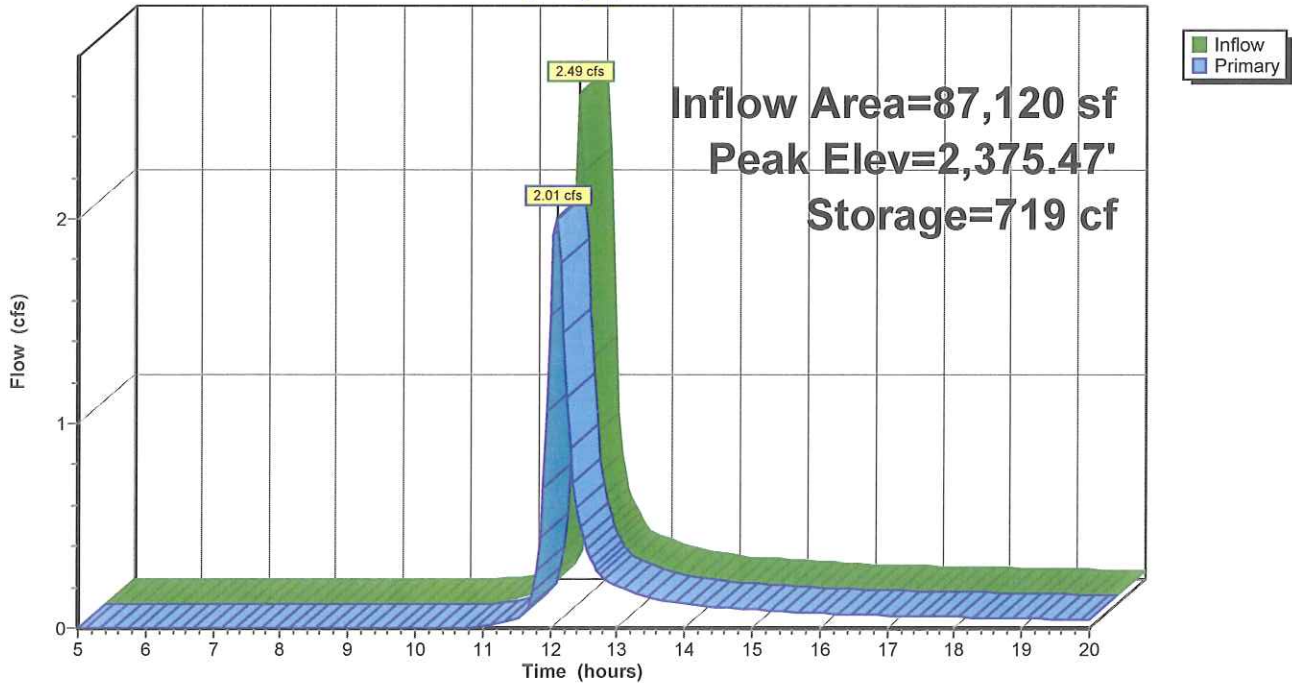
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	2,091 cf	3.00'W x 345.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.98 cfs @ 12.09 hrs HW=2,375.47' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 1.98 cfs @ 2.23 fps)

**Pond 2P: SWALE B**

Hydrograph



# RASPBERRY ACRES POST B

Type II 24-hr 100-YR Rainfall=2.40"

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## Summary for Pond 2P: SWALE B

Inflow Area = 87,120 sf, 38.00% Impervious, Inflow Depth > 0.89" for 100-YR event  
 Inflow = 2.95 cfs @ 12.02 hrs, Volume= 6,485 cf  
 Outflow = 2.38 cfs @ 12.09 hrs, Volume= 6,444 cf, Atten= 19%, Lag= 3.9 min  
 Primary = 2.38 cfs @ 12.09 hrs, Volume= 6,444 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.53' @ 12.09 hrs Surf.Area= 2,149 sf Storage= 841 cf

Plug-Flow detention time= 8.5 min calculated for 6,423 cf (99% of inflow)  
 Center-of-Mass det. time= 6.0 min ( 807.3 - 801.3 )

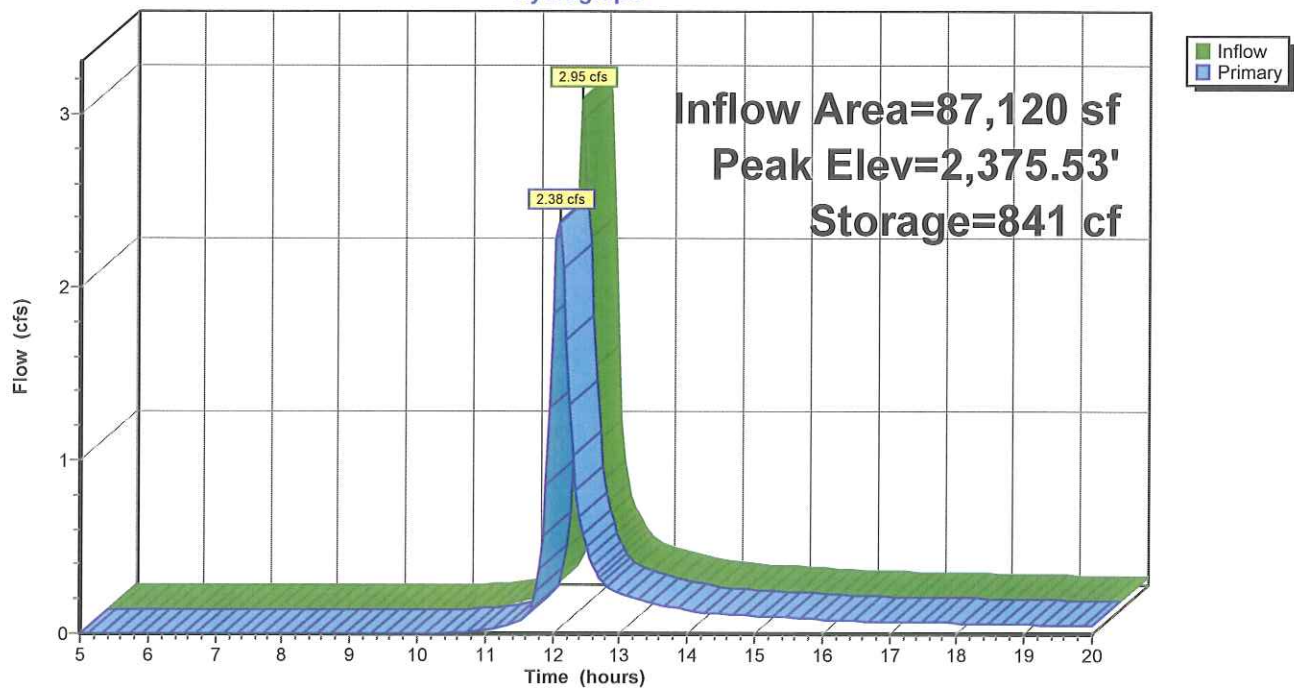
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	2,091 cf	3.00'W x 345.00'L x 1.00'H Prismaoid Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=2.35 cfs @ 12.09 hrs HW=2,375.52' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 2.35 cfs @ 2.37 fps)

## Pond 2P: SWALE B

Hydrograph



**BASIN "C"**

Total Area = 14030 sf = 0.322 acres.

Roof Area

0

Paved Area (includes curb & gutter)

(310' x 18.5') = 5735 Ft<sup>2</sup>

Total Paved Area = 5735 Ft<sup>2</sup> = 0.33 acres

C=0.90

Concrete Driveways & Sidewalk

310' x 5' = 1550 Ft<sup>2</sup>

C=0.90

Lawns

14030 – 7285 = 6745

C=0.15

Weighted "C" Factor

(0.9 x 7285) + (0.15 x 6745) divided by 14030

**= 0.54**

Required Swale Volume

V = 1815 A, where

V= Volume of swale (cubic feet)

A= Pollution generating impervious surface (acres)

V = 1815 x 0.1316 acres

**=239 CF**

Provided swale volume = 545 CF

Swale Along NE Orchard Ct.	
Pond Side Slope	3 :1
Bottom Length (ft)	240
Bottom Width (ft)	3
Bottom Area (SF)	720
Treatment Depth (ft)	0.5
Treatment Area (SF)	1458
Treatment Volume (CF)	545
Storage Depth (ft)	1
Storage Area (SF)	2214
Storage Volume (CF)	1467

**RASPBERRY ACRES POST C**

Type II 24-hr 2-YR Rainfall=1.60"

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**Summary for Pond 2P: SWALE C**

Inflow Area = 14,026 sf, 38.00% Impervious, Inflow Depth > 0.39" for 2-YR event  
 Inflow = 0.26 cfs @ 11.95 hrs, Volume= 458 cf  
 Outflow = 0.19 cfs @ 12.01 hrs, Volume= 453 cf, Atten= 28%, Lag= 3.4 min  
 Primary = 0.19 cfs @ 12.01 hrs, Volume= 453 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.09' @ 12.01 hrs Surf.Area= 858 sf Storage= 74 cf

Plug-Flow detention time= 12.1 min calculated for 452 cf (99% of inflow)  
 Center-of-Mass det. time= 8.3 min ( 822.7 - 814.5 )

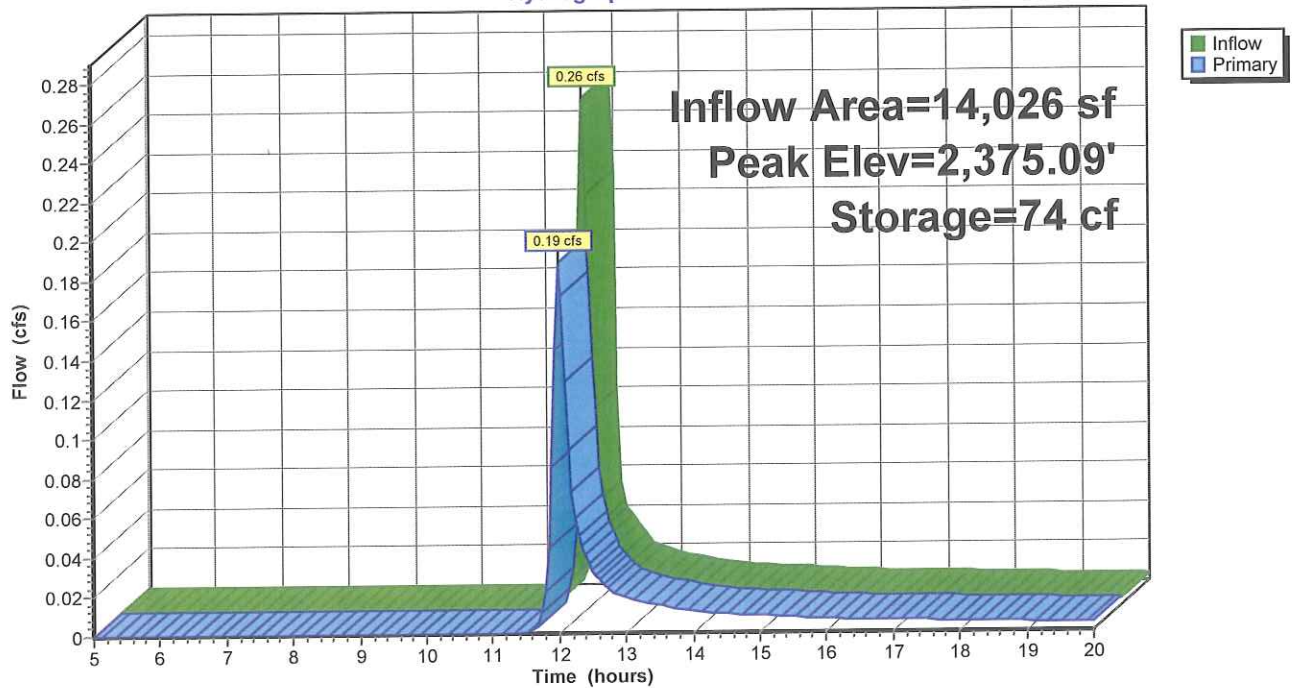
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,461 cf	3.00'W x 240.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.18 cfs @ 12.01 hrs HW=2,375.09' (Free Discharge)  
 ↳ Sharp-Crested Rectangular Weir (Weir Controls 0.18 cfs @ 0.99 fps)

**Pond 2P: SWALE C**

Hydrograph





# RASPBERRY ACRES POST C

Type II 24-hr 10-YR Rainfall=1.80"

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## Summary for Pond 2P: SWALE C

Inflow Area = 14,026 sf, 38.00% Impervious, Inflow Depth > 0.51" for 10-YR event  
 Inflow = 0.34 cfs @ 11.95 hrs, Volume= 592 cf  
 Outflow = 0.25 cfs @ 12.01 hrs, Volume= 587 cf, Atten= 25%, Lag= 3.2 min  
 Primary = 0.25 cfs @ 12.01 hrs, Volume= 587 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.12' @ 12.01 hrs Surf.Area= 889 sf Storage= 93 cf

Plug-Flow detention time= 11.2 min calculated for 585 cf (99% of inflow)  
 Center-of-Mass det. time= 7.6 min ( 816.3 - 808.7 )

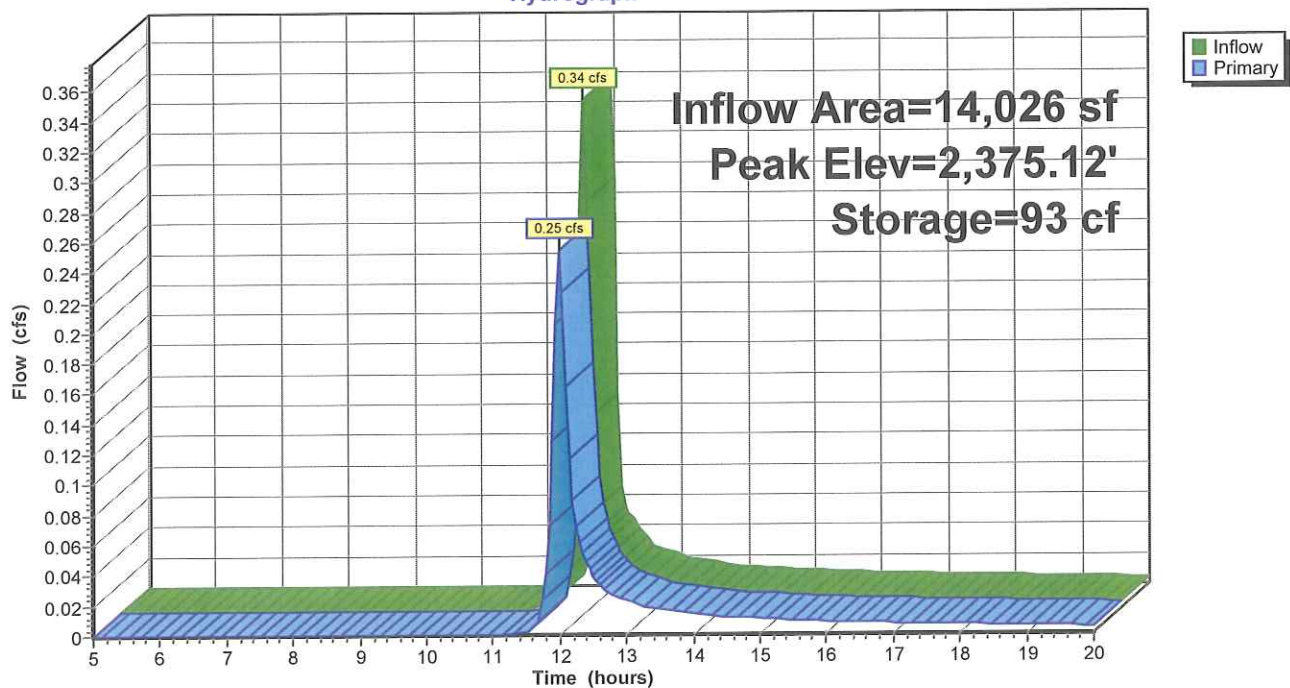
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,461 cf	3.00'W x 240.00'L x 1.00'H Prismaoid Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.25 cfs @ 12.01 hrs HW=2,375.11' (Free Discharge)  
 ↑1=Sharp-Crested Rectangular Weir (Weir Controls 0.25 cfs @ 1.11 fps)

## Pond 2P: SWALE C

Hydrograph



**RASPBERRY ACRES POST C**

Type II 24-hr 50-YR Rainfall=2.20"

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**Summary for Pond 2P: SWALE C**

Inflow Area = 14,026 sf, 38.00% Impervious, Inflow Depth > 0.76" for 50-YR event  
 Inflow = 0.51 cfs @ 11.95 hrs, Volume= 888 cf  
 Outflow = 0.40 cfs @ 12.00 hrs, Volume= 880 cf, Atten= 21%, Lag= 3.0 min  
 Primary = 0.40 cfs @ 12.00 hrs, Volume= 880 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.16' @ 12.00 hrs Surf.Area= 949 sf Storage= 130 cf

Plug-Flow detention time= 10.0 min calculated for 880 cf (99% of inflow)  
 Center-of-Mass det. time= 6.7 min ( 806.8 - 800.1 )

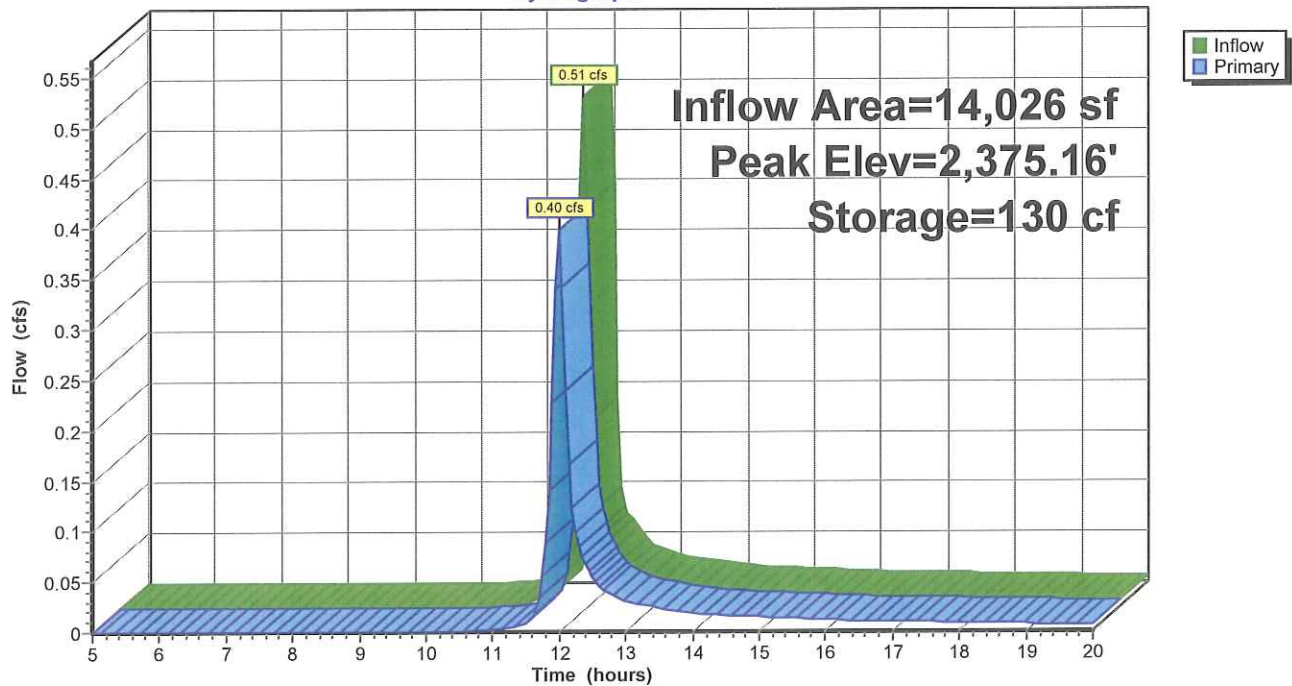
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,461 cf	3.00'W x 240.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.40 cfs @ 12.00 hrs HW=2,375.16' (Free Discharge)  
 ↑1=Sharp-Crested Rectangular Weir (Weir Controls 0.40 cfs @ 1.29 fps)

**Pond 2P: SWALE C**

Hydrograph





**RASPBERRY ACRES POST C**

Type II 24-hr 100-YR Rainfall=2.40"

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**Summary for Pond 2P: SWALE C**

Inflow Area = 14,026 sf, 38.00% Impervious, Inflow Depth > 0.90" for 100-YR event  
 Inflow = 0.60 cfs @ 11.95 hrs, Volume= 1,047 cf  
 Outflow = 0.47 cfs @ 12.00 hrs, Volume= 1,039 cf, Atten= 20%, Lag= 2.9 min  
 Primary = 0.47 cfs @ 12.00 hrs, Volume= 1,039 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.18' @ 12.00 hrs Surf.Area= 978 sf Storage= 149 cf

Plug-Flow detention time= 9.5 min calculated for 1,035 cf (99% of inflow)  
 Center-of-Mass det. time= 6.5 min ( 803.1 - 796.6 )

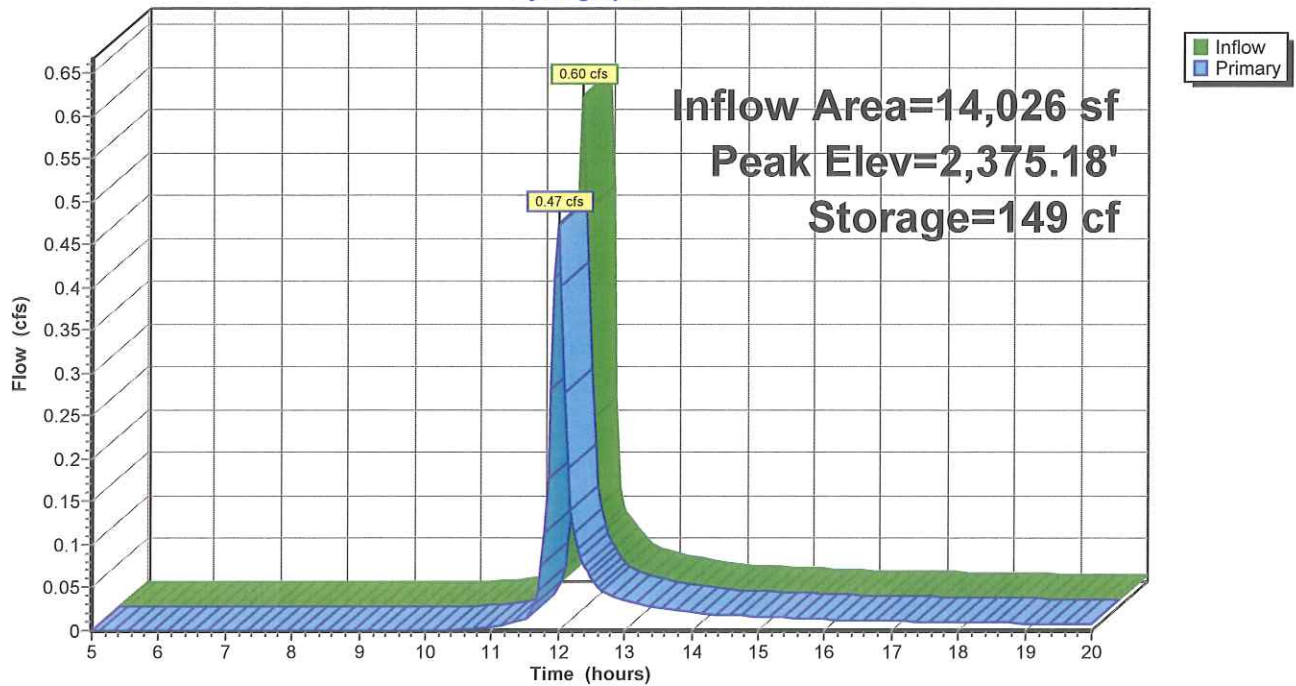
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,461 cf	3.00'W x 240.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.47 cfs @ 12.00 hrs HW=2,375.18' (Free Discharge)  
 1=Sharp-Crested Rectangular Weir (Weir Controls 0.47 cfs @ 1.37 fps)

**Pond 2P: SWALE C**

Hydrograph



**BASIN "D"**

Total Area = 43225 sf = 0.99 acres.

Roof Area

$$(2000 \text{ sf} \times 4) = 8,000 \text{ sf} \quad C=0.90$$

Paved Area (includes curb & gutter)

$$(355' \times 18.5') + 4000 = 10,570 \text{ Ft}^2$$

$$\text{Total Paved Area} = 10,570 \text{ Ft}^2 \quad C=0.90$$

Concrete Driveways & Sidewalk

$$\begin{aligned} 500\text{sf} \times 4 &= 2000 \text{ Ft}^2 \\ 160' \times 5' &= 800 \text{ Ft}^2 \end{aligned} \quad C=0.90$$

Lawns

$$43225 - 21370 = 21855 \text{ sf} \quad C=0.15$$

Weighted "C" Factor

$$(0.9 \times 21370) + (0.15 \times 21855) \text{ divided by } 43225$$

$$= 0.52$$

Required Swale Volume

V = 1815 A, where

V= Volume of swale (cubic feet)

A= Pollution generating impervious surface (acres)

$$V = 1815 \times 0.289 \text{ acres}$$

$$= 524 \text{ CF}$$

Provided swale volume = 567 CF

Swale Along SE Orchard CT.	
Pond Side Slope	3 :1
Bottom Length (ft)	250
Bottom Width (ft)	3
Bottom Area (SF)	750
Treatment Depth (ft)	0.5
Treatment Area (SF)	1518
Treatment Volume (CF)	567
Storage Depth (ft)	1
Storage Area (SF)	2304
Storage Volume (CF)	1527

**RASPBERRY ACRES POST D**

Type II 24-hr 2-YR Rainfall=1.60"

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**Summary for Pond 2P: SWALE D**

Inflow Area = 43,124 sf, 38.00% Impervious, Inflow Depth > 0.39" for 2-YR event  
 Inflow = 0.74 cfs @ 11.98 hrs, Volume= 1,407 cf  
 Outflow = 0.58 cfs @ 12.03 hrs, Volume= 1,395 cf, Atten= 21%, Lag= 3.1 min  
 Primary = 0.58 cfs @ 12.03 hrs, Volume= 1,395 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.20' @ 12.03 hrs Surf.Area= 1,058 sf Storage= 183 cf

Plug-Flow detention time= 9.1 min calculated for 1,390 cf (99% of inflow)  
 Center-of-Mass det. time= 6.0 min ( 821.9 - 815.9 )

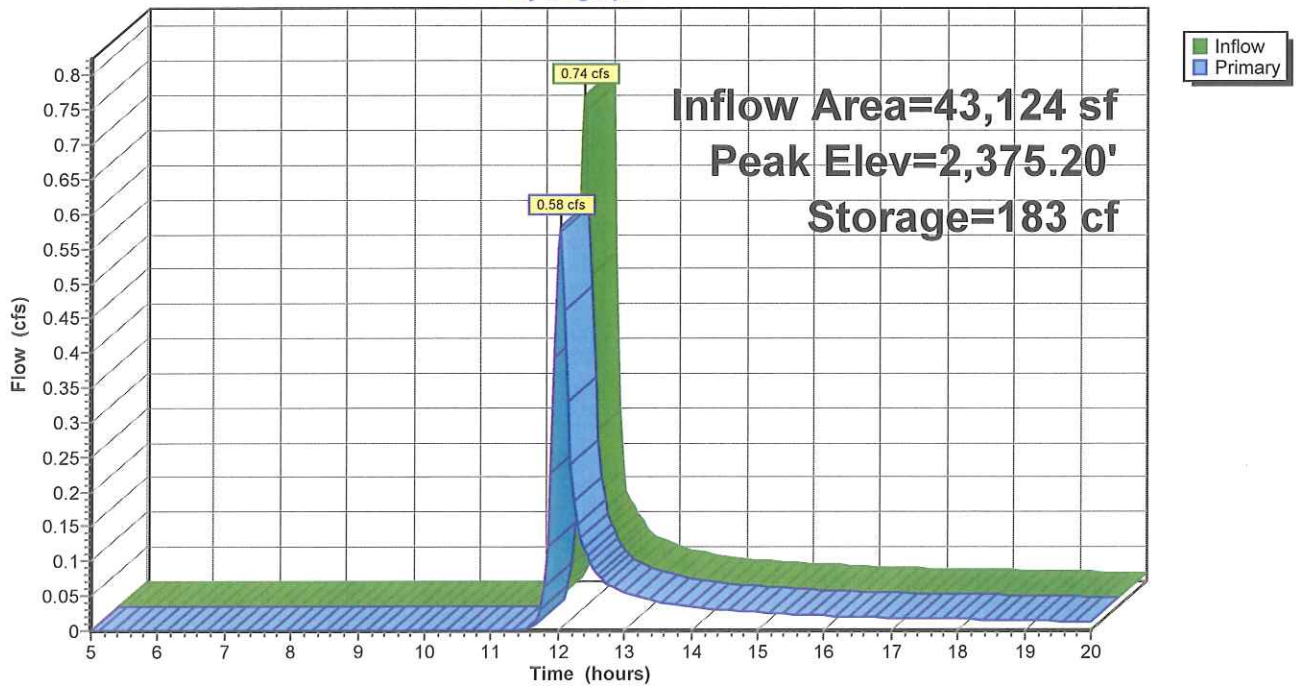
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,521 cf	3.00'W x 250.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.57 cfs @ 12.03 hrs HW=2,375.20' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 0.57 cfs @ 1.46 fps)

**Pond 2P: SWALE D**

Hydrograph



**RASPBERRY ACRES POST D**

Type II 24-hr 10-YR Rainfall=1.80"

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**Summary for Pond 2P: SWALE D**

Inflow Area = 43,124 sf, 38.00% Impervious, Inflow Depth > 0.51" for 10-YR event  
 Inflow = 0.96 cfs @ 11.98 hrs, Volume= 1,819 cf  
 Outflow = 0.77 cfs @ 12.03 hrs, Volume= 1,806 cf, Atten= 19%, Lag= 2.9 min  
 Primary = 0.77 cfs @ 12.03 hrs, Volume= 1,806 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.25' @ 12.03 hrs Surf.Area= 1,125 sf Storage= 230 cf

Plug-Flow detention time= 8.5 min calculated for 1,806 cf (99% of inflow)  
 Center-of-Mass det. time= 5.6 min ( 815.8 - 810.2 )

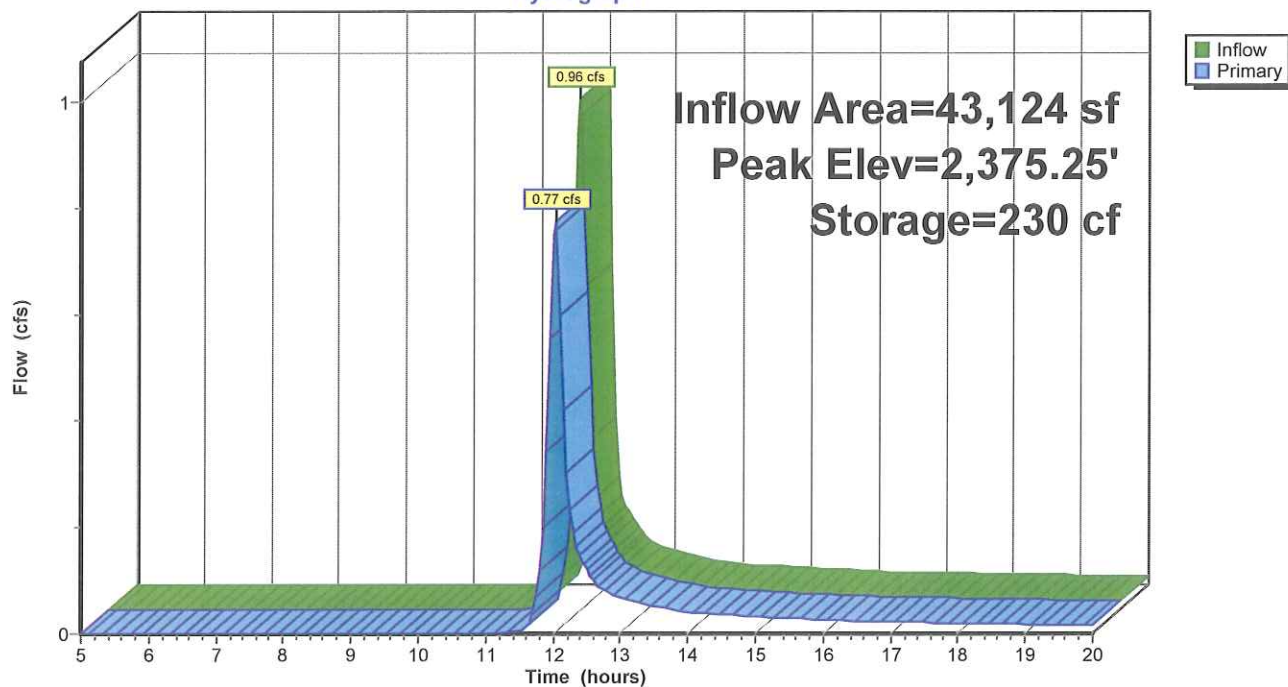
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,521 cf	3.00'W x 250.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.75 cfs @ 12.03 hrs HW=2,375.24' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 0.75 cfs @ 1.60 fps)

**Pond 2P: SWALE D**

Hydrograph





**RASPBERRY ACRES POST D**

Type II 24-hr 50-YR Rainfall=2.20"

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**Summary for Pond 2P: SWALE D**

Inflow Area = 43,124 sf, 38.00% Impervious, Inflow Depth > 0.76" for 50-YR event  
 Inflow = 1.44 cfs @ 11.98 hrs, Volume= 2,728 cf  
 Outflow = 1.19 cfs @ 12.02 hrs, Volume= 2,711 cf, Atten= 17%, Lag= 2.7 min  
 Primary = 1.19 cfs @ 12.02 hrs, Volume= 2,711 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.33' @ 12.02 hrs Surf.Area= 1,254 sf Storage= 330 cf

Plug-Flow detention time= 7.6 min calculated for 2,711 cf (99% of inflow)  
 Center-of-Mass det. time= 5.2 min ( 806.8 - 801.5 )

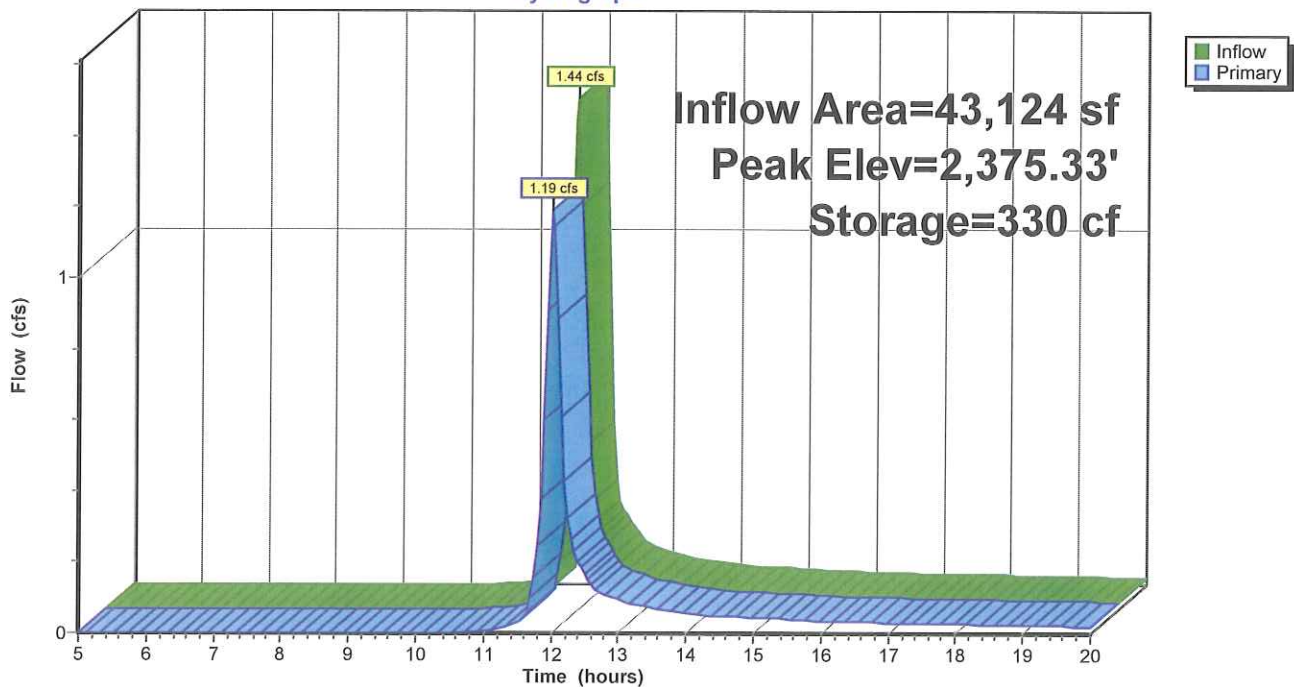
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,521 cf	3.00'W x 250.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.16 cfs @ 12.02 hrs HW=2,375.32' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 1.16 cfs @ 1.86 fps)

**Pond 2P: SWALE D**

Hydrograph



**RASPBERRY ACRES POST D**

Type II 24-hr 100-YR Rainfall=2.40"

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**Summary for Pond 2P: SWALE D**

Inflow Area = 43,124 sf, 38.00% Impervious, Inflow Depth > 0.89" for 100-YR event  
 Inflow = 1.68 cfs @ 11.97 hrs, Volume= 3,215 cf  
 Outflow = 1.41 cfs @ 12.02 hrs, Volume= 3,197 cf, Atten= 16%, Lag= 2.7 min  
 Primary = 1.41 cfs @ 12.02 hrs, Volume= 3,197 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.37' @ 12.02 hrs Surf.Area= 1,316 sf Storage= 382 cf

Plug-Flow detention time= 7.3 min calculated for 3,187 cf (99% of inflow)  
 Center-of-Mass det. time= 5.1 min ( 803.2 - 798.1 )

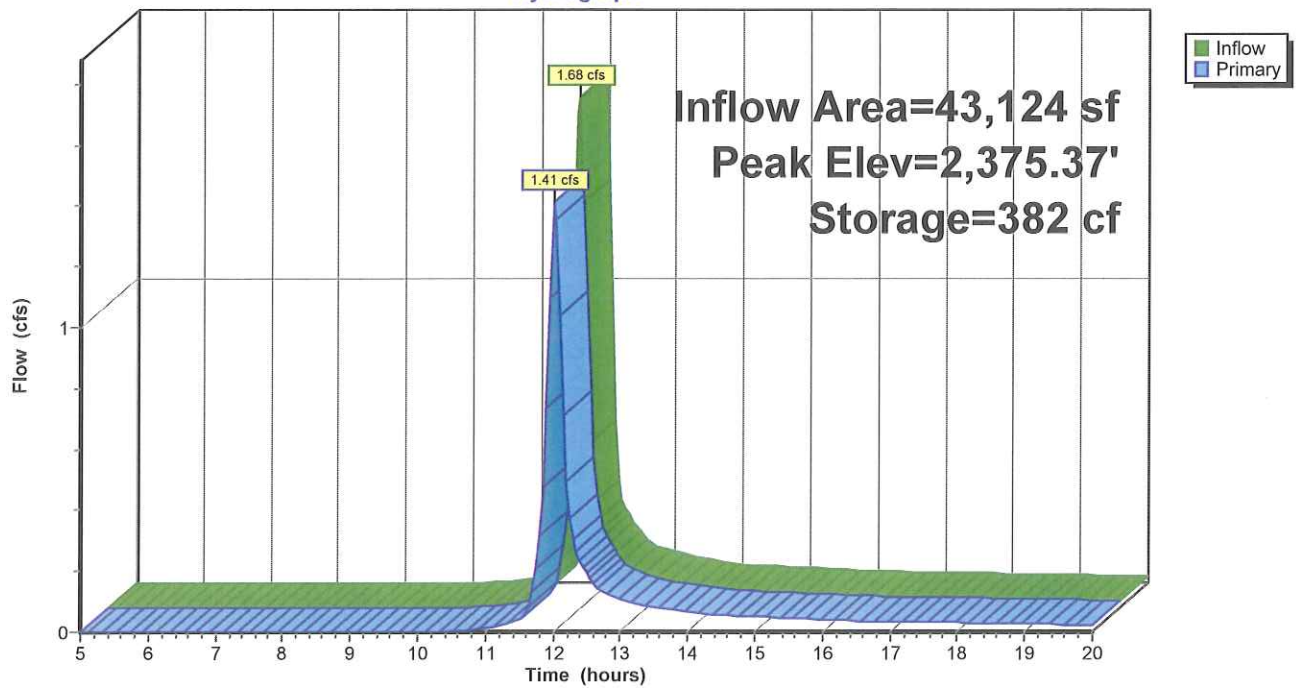
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,521 cf	3.00'W x 250.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.38 cfs @ 12.02 hrs HW=2,375.36' (Free Discharge)  
 ↳ 1=Sharp-Crested Rectangular Weir (Weir Controls 1.38 cfs @ 1.97 fps)

**Pond 2P: SWALE D**

Hydrograph





**BASIN "E"**

Total Area = 42000 sf = 0.964 acres.

Roof Area

(2000 sf x 4) = 8,000 sf C=0.90

Paved Area (includes curb & gutter)

(480' x 18.5') = 8880 Ft<sup>2</sup> C=0.90

Concrete Driveways & Sidewalk

500sf x 4 = 2000 Ft<sup>2</sup> C=0.90  
 408' x 5' = 2040 Ft<sup>2</sup>

Lawns

42000 – 20920 = 21080 sf C=0.15

Weighted "C" Factor

(0.9 x 20920) + (0.15 x 21080) divided by 42000  
**= 0.52**

Required Swale Volume

V = 1815 A, where  
 V= Volume of swale (cubic feet)  
 A= Pollution generating impervious surface (acres)

V = 1815 x 0.25 acres  
**=453 CF**

Provided swale volume = 905 CF

Swale Along North Walker Ave.	
Pond Side Slope	3 :1
Bottom Length (ft)	400
Bottom Width (ft)	3
Bottom Area (SF)	1200
Treatment Depth (ft)	0.5
Treatment Area (SF)	2418
Treatment Volume (CF)	905
Storage Depth (ft)	1
Storage Area (SF)	3654
Storage Volume (CF)	2427

**RASPBERRY ACRES POST E**

Type II 24-hr 2-YR Rainfall=1.60"

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Page 1

**Summary for Pond 2P: SWALE E**

Inflow Area = 41,992 sf, 38.00% Impervious, Inflow Depth > 0.39" for 2-YR event  
 Inflow = 0.55 cfs @ 12.06 hrs, Volume= 1,365 cf  
 Outflow = 0.40 cfs @ 12.15 hrs, Volume= 1,347 cf, Atten= 28%, Lag= 5.5 min  
 Primary = 0.40 cfs @ 12.15 hrs, Volume= 1,347 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.16' @ 12.15 hrs Surf.Area= 1,581 sf Storage= 219 cf

Plug-Flow detention time= 14.7 min calculated for 1,342 cf (98% of inflow)  
 Center-of-Mass det. time= 9.7 min ( 830.5 - 820.7 )

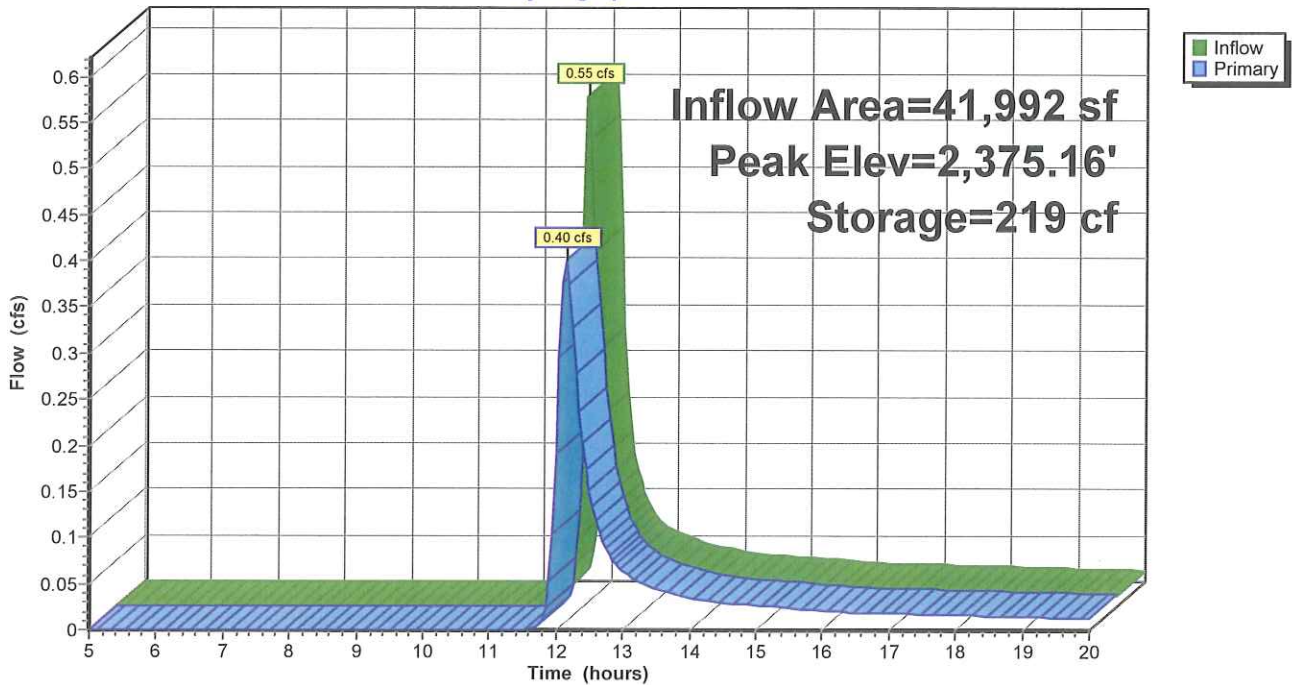
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	2,421 cf	3.00'W x 400.00'L x 1.00'H Prismaoid Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.40 cfs @ 12.15 hrs HW=2,375.16' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 0.40 cfs @ 1.30 fps)

**Pond 2P: SWALE E**

Hydrograph



**RASPBERRY ACRES POST E**

Type II 24-hr 10-YR Rainfall=1.80"

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**Summary for Pond 2P: SWALE E**

Inflow Area = 41,992 sf, 38.00% Impervious, Inflow Depth > 0.50" for 10-YR event  
 Inflow = 0.73 cfs @ 12.05 hrs, Volume= 1,766 cf  
 Outflow = 0.55 cfs @ 12.14 hrs, Volume= 1,745 cf, Atten= 25%, Lag= 5.2 min  
 Primary = 0.55 cfs @ 12.14 hrs, Volume= 1,745 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.19' @ 12.14 hrs Surf.Area= 1,669 sf Storage= 278 cf

Plug-Flow detention time= 13.7 min calculated for 1,745 cf (99% of inflow)  
 Center-of-Mass det. time= 9.1 min ( 824.2 - 815.1 )

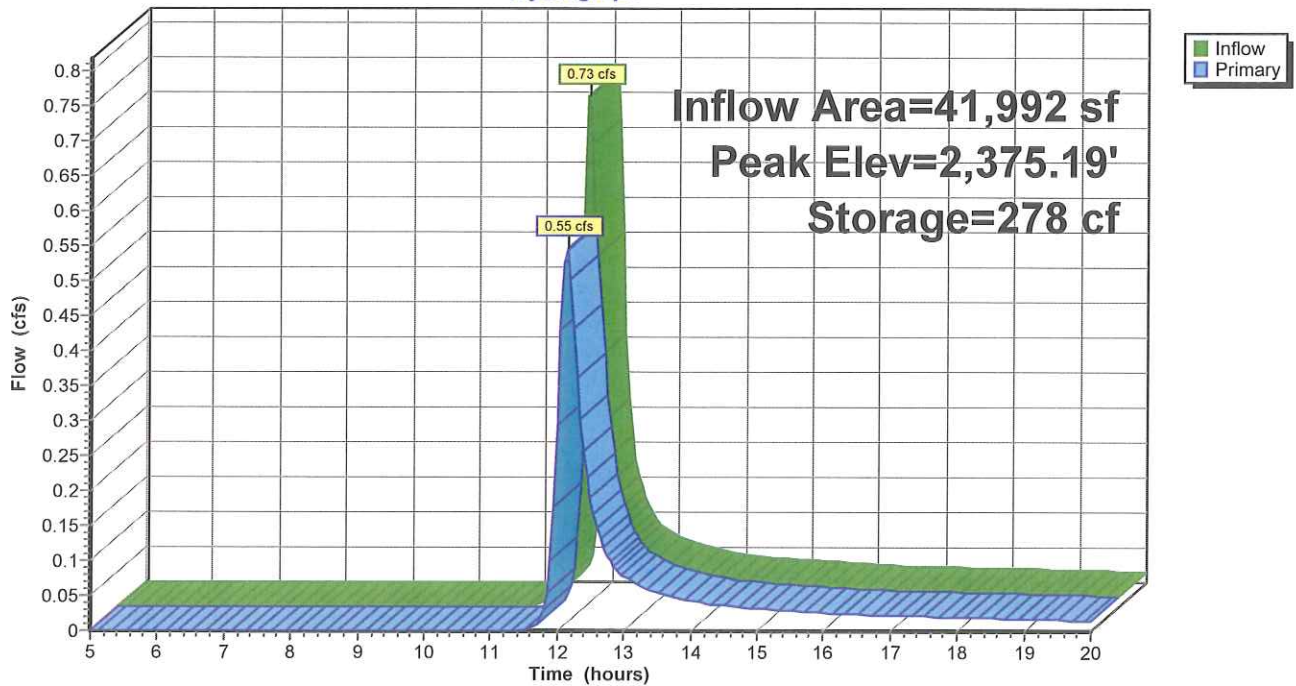
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	2,421 cf	3.00'W x 400.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.54 cfs @ 12.14 hrs HW=2,375.19' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 0.54 cfs @ 1.43 fps)

**Pond 2P: SWALE E**

Hydrograph



# RASPBERRY ACRES POST E

Type II 24-hr 50-YR Rainfall=2.20"

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## Summary for Pond 2P: SWALE E

Inflow Area = 41,992 sf, 38.00% Impervious, Inflow Depth > 0.76" for 50-YR event  
 Inflow = 1.11 cfs @ 12.05 hrs, Volume= 2,649 cf  
 Outflow = 0.86 cfs @ 12.13 hrs, Volume= 2,622 cf, Atten= 22%, Lag= 4.7 min  
 Primary = 0.86 cfs @ 12.13 hrs, Volume= 2,622 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.26' @ 12.13 hrs Surf.Area= 1,839 sf Storage= 400 cf

Plug-Flow detention time= 12.2 min calculated for 2,614 cf (99% of inflow)  
 Center-of-Mass det. time= 8.4 min ( 814.9 - 806.5 )

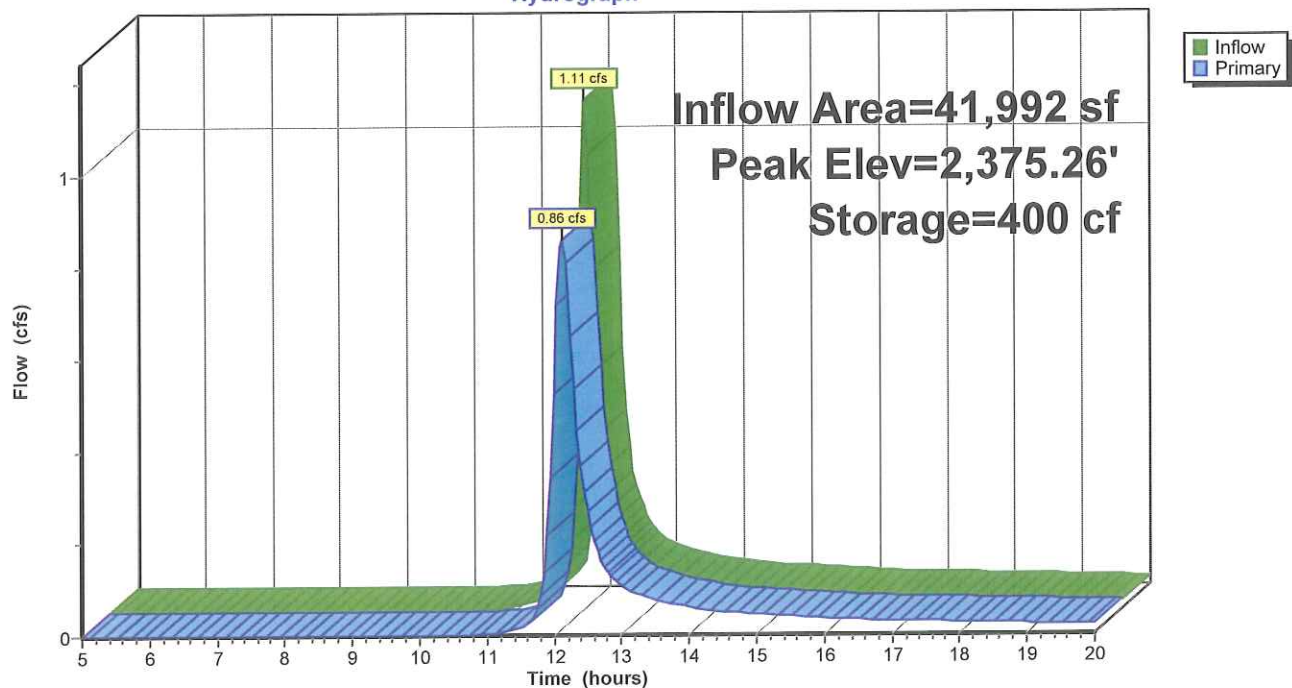
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	2,421 cf	3.00'W x 400.00'L x 1.00'H Prismaoid Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.85 cfs @ 12.13 hrs HW=2,375.26' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 0.85 cfs @ 1.67 fps)

## Pond 2P: SWALE E

Hydrograph





**RASPBERRY ACRES POST E**

Type II 24-hr 100-YR Rainfall=2.40"

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**Summary for Pond 2P: SWALE E**

Inflow Area = 41,992 sf, 38.00% Impervious, Inflow Depth > 0.89" for 100-YR event  
 Inflow = 1.31 cfs @ 12.05 hrs, Volume= 3,123 cf  
 Outflow = 1.03 cfs @ 12.13 hrs, Volume= 3,094 cf, Atten= 22%, Lag= 4.6 min  
 Primary = 1.03 cfs @ 12.13 hrs, Volume= 3,094 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.30' @ 12.13 hrs Surf.Area= 1,921 sf Storage= 463 cf

Plug-Flow detention time= 11.8 min calculated for 3,094 cf (99% of inflow)  
 Center-of-Mass det. time= 8.2 min ( 811.3 - 803.1 )

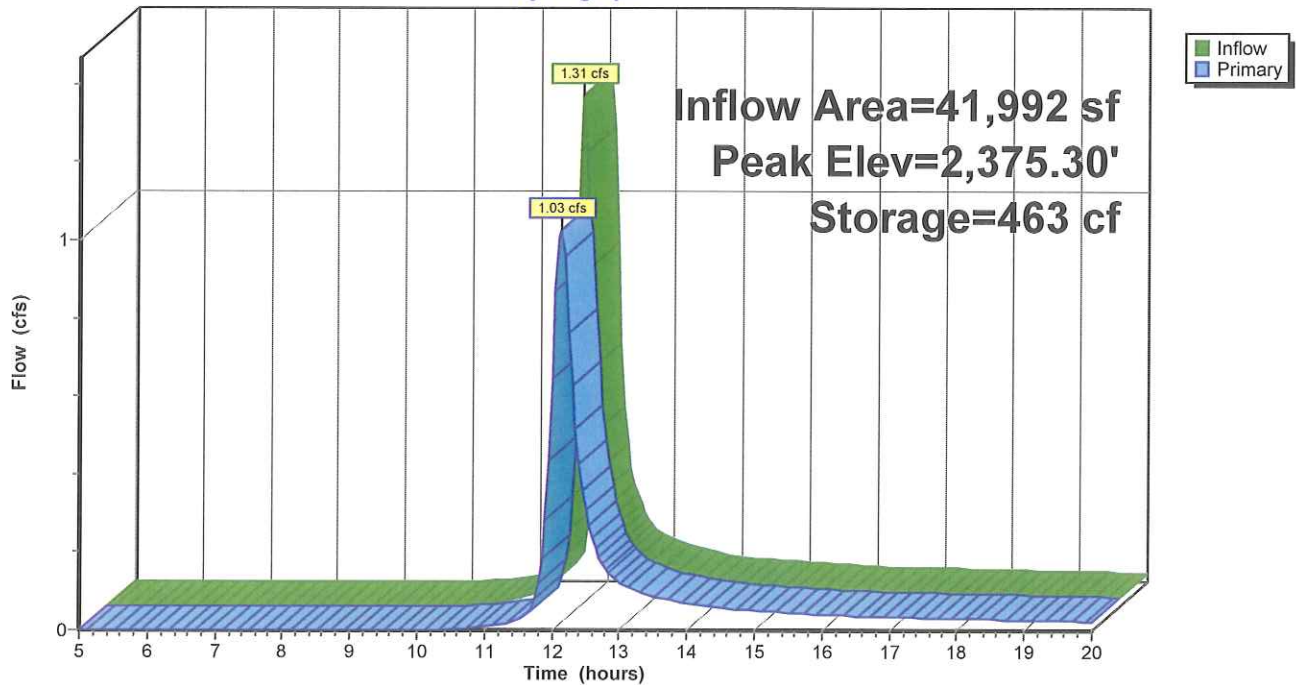
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	2,421 cf	3.00'W x 400.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.01 cfs @ 12.13 hrs HW=2,375.29' (Free Discharge)  
 ↑1=Sharp-Crested Rectangular Weir (Weir Controls 1.01 cfs @ 1.77 fps)

**Pond 2P: SWALE E**

Hydrograph



**BASIN "F"**



Total Area = 74470 sf = 1.71 acres.

Roof Area

$$(2000 \text{ sf} \times 9) = 18,000 \text{ sf} \quad C=0.90$$

Paved Area (includes curb & gutter)

$$(480' \times 18.5') = 8880 \text{ Ft}^2 \quad C=0.90$$

Concrete Driveways & Sidewalk

$$500\text{sf} \times 9 = 4500 \text{ Ft}^2 \quad C=0.90$$

$$318' \times 5' = 1590 \text{ Ft}^2$$

Lawns

$$74470 - 32970 = 41500 \text{ sf} \quad C=0.15$$

Weighted "C" Factor

$$(0.9 \times 32970) + (0.15 \times 41500) \text{ divided by } 74470$$

$$= 0.48$$

Required Swale Volume

V = 1815 A, where

V= Volume of swale (cubic feet)

A= Pollution generating impervious surface (acres)

$$V = 1815 \times 0.31 \text{ acres}$$

$$=558 \text{ CF}$$

Provided swale volume = 720 CF

Swale Along South Walker Ave.	
Pond Side Slope	3 :1
Bottom Length (ft)	318
Bottom Width (ft)	3
Bottom Area (SF)	954
Treatment Depth (ft)	0.5
Treatment Area (SF)	1926
Treatment Volume (CF)	720
Storage Depth (ft)	1
Storage Area (SF)	2916
Storage Volume (CF)	1935

**RASPBERRY ACRES POST F**

Type II 24-hr 2-YR Rainfall=1.60"

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**Summary for Pond 2P: SWALE F**

Inflow Area = 74,488 sf, 38.00% Impervious, Inflow Depth > 0.39" for 2-YR event  
 Inflow = 0.97 cfs @ 12.06 hrs, Volume= 2,421 cf  
 Outflow = 0.79 cfs @ 12.13 hrs, Volume= 2,399 cf, Atten= 19%, Lag= 4.3 min  
 Primary = 0.79 cfs @ 12.13 hrs, Volume= 2,399 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.25' @ 12.13 hrs Surf.Area= 1,433 sf Storage= 296 cf

Plug-Flow detention time= 9.9 min calculated for 2,391 cf (99% of inflow)  
 Center-of-Mass det. time= 6.6 min ( 827.6 - 821.0 )

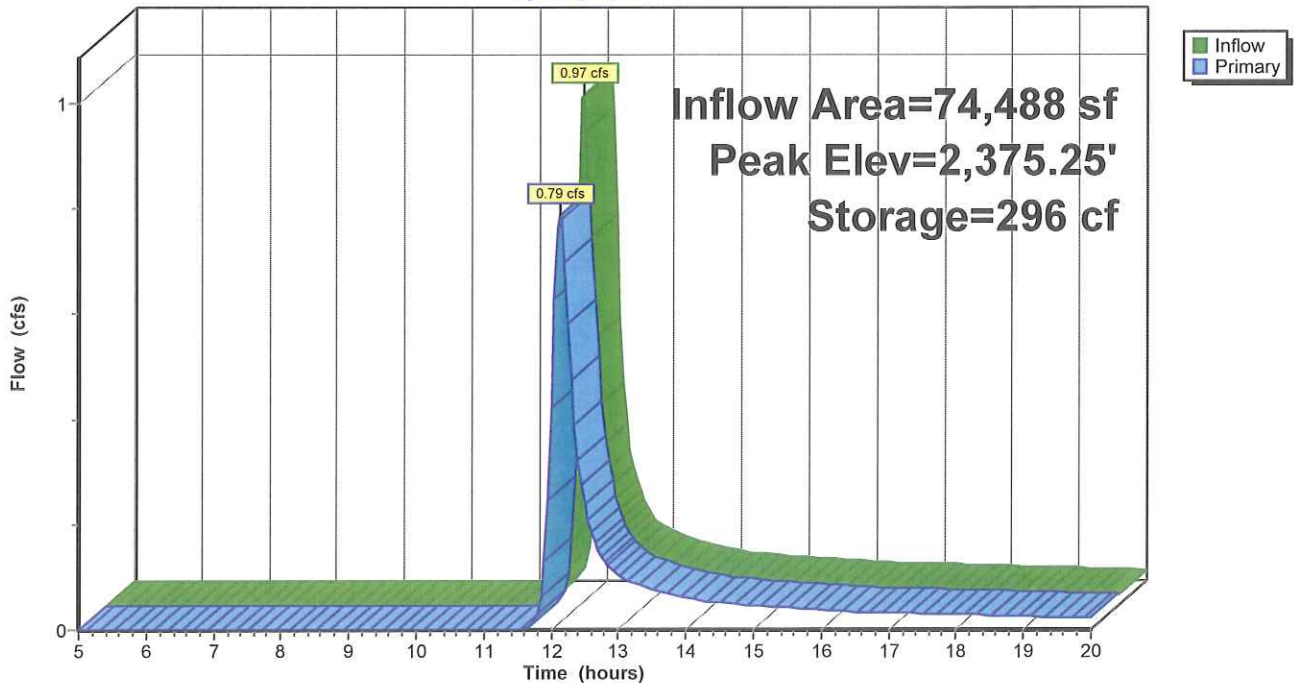
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,929 cf	3.00'W x 318.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.78 cfs @ 12.13 hrs HW=2,375.25' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 0.78 cfs @ 1.62 fps)

**Pond 2P: SWALE F**

Hydrograph



# RASPBERRY ACRES POST F

Type II 24-hr 10-YR Rainfall=1.80"

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## Summary for Pond 2P: SWALE F

Inflow Area = 74,488 sf, 38.00% Impervious, Inflow Depth > 0.50" for 10-YR event  
 Inflow = 1.28 cfs @ 12.06 hrs, Volume= 3,132 cf  
 Outflow = 1.05 cfs @ 12.13 hrs, Volume= 3,108 cf, Atten= 18%, Lag= 4.1 min  
 Primary = 1.05 cfs @ 12.13 hrs, Volume= 3,108 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.30' @ 12.13 hrs Surf.Area= 1,539 sf Storage= 377 cf

Plug-Flow detention time= 9.3 min calculated for 3,108 cf (99% of inflow)  
 Center-of-Mass det. time= 6.3 min ( 821.6 - 815.3 )

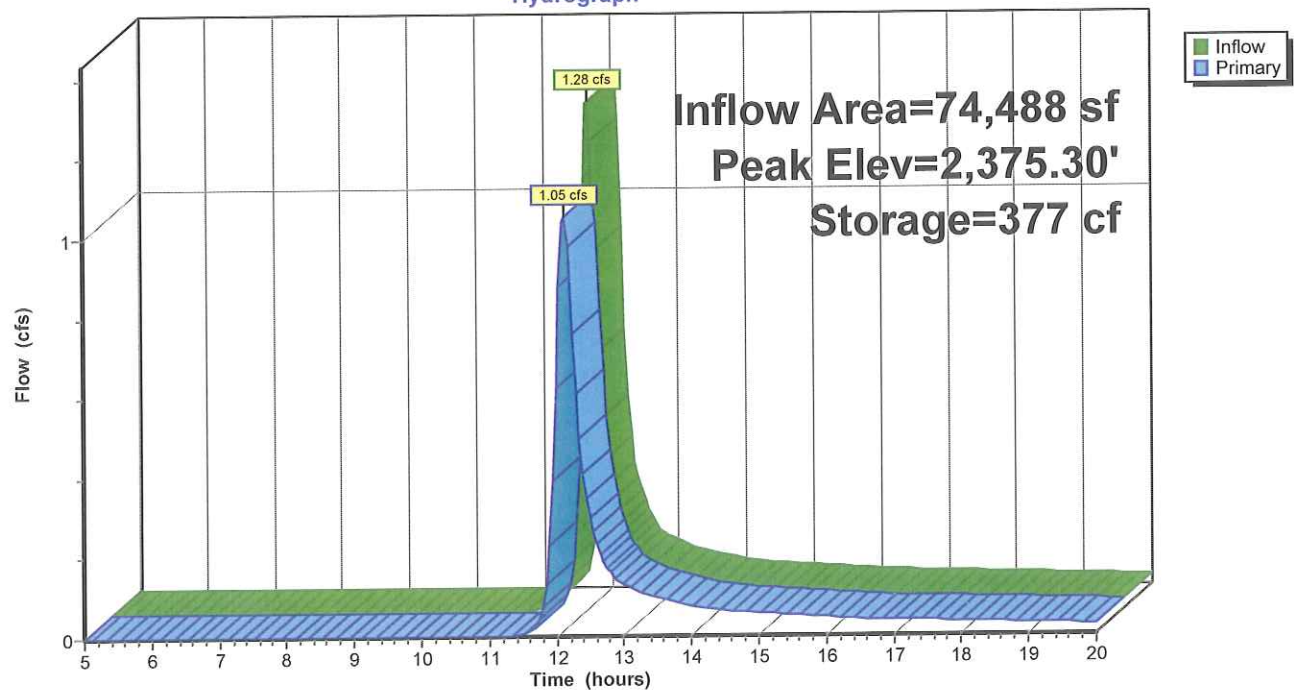
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,929 cf	3.00'W x 318.00'L x 1.00'H Prismaoid Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.04 cfs @ 12.13 hrs HW=2,375.30' (Free Discharge)  
 ↑1=Sharp-Crested Rectangular Weir (Weir Controls 1.04 cfs @ 1.79 fps)

## Pond 2P: SWALE F

Hydrograph



**RASPBERRY ACRES POST F**

Type II 24-hr 50-YR Rainfall=2.20"

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**Summary for Pond 2P: SWALE F**

Inflow Area = 74,488 sf, 38.00% Impervious, Inflow Depth > 0.76" for 50-YR event  
 Inflow = 1.95 cfs @ 12.05 hrs, Volume= 4,698 cf  
 Outflow = 1.64 cfs @ 12.12 hrs, Volume= 4,667 cf, Atten= 16%, Lag= 3.9 min  
 Primary = 1.64 cfs @ 12.12 hrs, Volume= 4,667 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.41' @ 12.12 hrs Surf.Area= 1,746 sf Storage= 551 cf

Plug-Flow detention time= 8.4 min calculated for 4,651 cf (99% of inflow)  
 Center-of-Mass det. time= 5.9 min ( 812.6 - 806.8 )

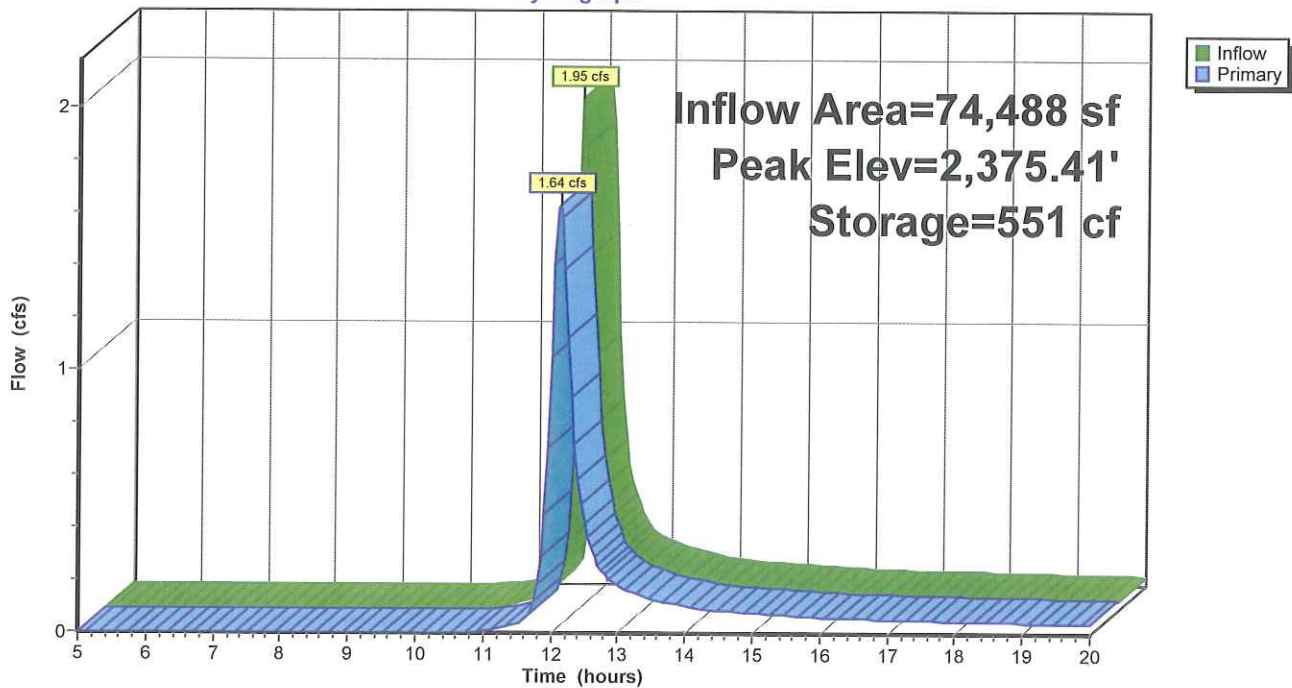
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,929 cf	3.00'W x 318.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.61 cfs @ 12.12 hrs HW=2,375.40' (Free Discharge)  
 ↳1=Sharp-Crested Rectangular Weir (Weir Controls 1.61 cfs @ 2.08 fps)

**Pond 2P: SWALE F**

Hydrograph





# RASPBERRY ACRES POST F

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Type II 24-hr 100-YR Rainfall=2.40"

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## Summary for Pond 2P: SWALE F

Inflow Area = 74,488 sf, 38.00% Impervious, Inflow Depth > 0.89" for 100-YR event  
 Inflow = 2.30 cfs @ 12.05 hrs, Volume= 5,538 cf  
 Outflow = 1.94 cfs @ 12.12 hrs, Volume= 5,505 cf, Atten= 16%, Lag= 3.9 min  
 Primary = 1.94 cfs @ 12.12 hrs, Volume= 5,505 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 2,375.46' @ 12.12 hrs Surf.Area= 1,846 sf Storage= 642 cf

Plug-Flow detention time= 8.1 min calculated for 5,505 cf (99% of inflow)  
 Center-of-Mass det. time= 5.7 min ( 809.1 - 803.4 )

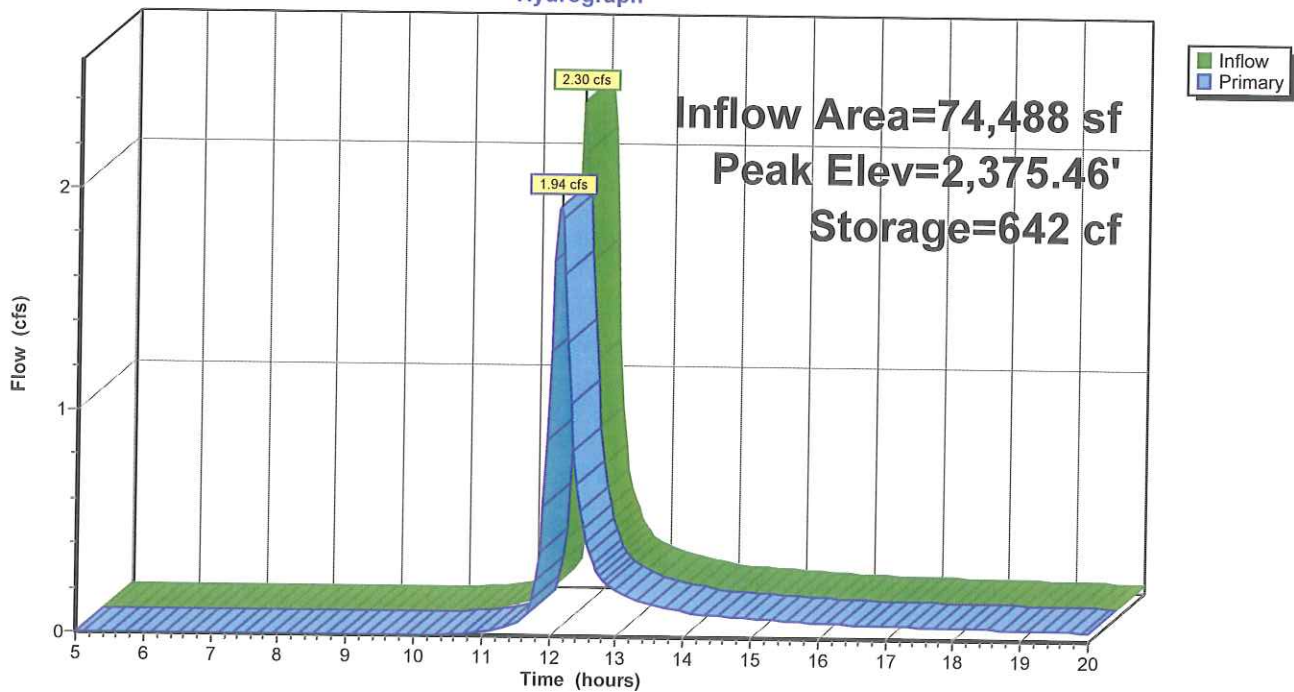
Volume	Invert	Avail.Storage	Storage Description
#1	2,375.00'	1,929 cf	3.00'W x 318.00'L x 1.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	2,375.00'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.91 cfs @ 12.12 hrs HW=2,375.45' (Free Discharge)  
 ↳ Sharp-Crested Rectangular Weir (Weir Controls 1.91 cfs @ 2.20 fps)

## Pond 2P: SWALE F

Hydrograph



**BASIN "G"**



Total Area = 13400 sf = 0.31 acres.

Roof Area

$$(2000 \text{ sf} \times 1) = 2,000 \text{ sf}$$

C=0.90

Paved Area (includes curb & gutter)

$$(222' \times 20.5') = 4551 \text{ Ft}^2$$

C=0.90

Concrete Driveways & Sidewalk

$$500\text{sf} \times 1 = 500 \text{ Ft}^2$$

$$140' \times 5' = 700 \text{ Ft}^2$$

C=0.90

Lawns

$$13400 - 7751 = 5649 \text{ sf}$$

C=0.15

Weighted "C" Factor

$$(0.9 \times 7751) + (0.15 \times 5649) \text{ divided by } 13400$$

$$= \mathbf{0.58}$$

Required Swale Volume

V = 1815 A, where

V= Volume of swale (cubic feet)

A= Pollution generating impervious surface (acres)

$$V = 1815 \times 0.116 \text{ acres}$$

$$= \mathbf{210 \text{ CF}}$$

Provided swale volume = 275 CF

Swale Along Austin	
Pond Side Slope	3 :1
Bottom Length (ft)	120
Bottom Width (ft)	3
Bottom Area (SF)	360
Treatment Depth (ft)	0.5
Treatment Area (SF)	738
Treatment Volume (CF)	275
Storage Depth (ft)	1
Storage Area (SF)	1134
Storage Volume (CF)	747